

**Traffic Impact and Access Study** 

# Cumberland Farms Convenience Store with Gasoline Sales

Westfield, Massachusetts

Prepared forFirst Hartford Realty Corporation149 Colonial RoadManchester, CT 06042

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# **1** Introduction

Vanasse Hangen Brustlin, Inc. (VHB) has completed a detailed Traffic Impact and Access Study to evaluate the traffic impacts associated with the development of a proposed Cumberland Farms Convenience Store with Gasoline Sales on an approximate 1.17 acre site. The site is located on the southwest corner of the intersection of Southampton Road (Route 10/202) at North Road (Route 202) in the City of Westfield, Massachusetts. The site location can be seen on Figure 1. The site is currently zoned Commercial.

VHB has evaluated existing traffic operations in the area, assessed the impacts of this development, and identified transportation improvements necessary to accommodate this redevelopment and potential traffic growth in this area.

## **Project Description**

The project site is currently undeveloped, and is primarily wooded. The proposed project consists of a Cumberland Farms convenience store and fueling facility with 5 gasoline pumps (10 vehicle fueling positions) as well as a convenience store. The proposed Cumberland Farms convenience store is approximately 4,513 ± square feet.

Access to the site will be provided via three access points; a full-access driveway and an entrance-only driveway located off Southampton Road (approximately 225 feet and 50 feet south of the intersection with North Road, respectively), and one fullaccess driveway located off North Road (approximately 115 feet west of the intersection with Southampton Road).

## **Study Methodology**

This traffic assessment has been conducted in the following manner. First, VHB assessed the existing traffic conditions within the project area including an inventory of existing roadway geometry, observations of traffic flow, peak period traffic counts, and a review of traffic safety in the area.





Then, the framework for evaluating the transportation impacts of the proposed project was established. Specific travel demand forecasts for the project were assessed along with future traffic demands on the study area roadways due to projected background traffic growth and other proposed area development that will occur independent of the proposed development. This traffic impact and access study has been prepared in accordance with the guidelines for traffic impact analysis set forth by the Executive Office of Energy and Environmental Affairs (EOEEA), Executive Office of Transportation and Public Works (EOTPW) and the Massachusetts Highway Department (MassDOT). In accordance with these guidelines, the year 2018 (a five-year time horizon), was selected as the design year for analysis. The traffic analysis conducted identified both existing and projected future roadway capacities and demands.



Evaluation of the transportation impacts associated with the proposed project requires a thorough understanding of the existing transportation conditions in the project study area. Existing transportation conditions in the study area include roadway geometry, traffic controls, traffic flow, and traffic safety data. Each of these elements is described in detail below.

## **Study Area**

To effectively evaluate the transportation impacts associated with the proposed development, it is necessary to review the existing roadway system in the vicinity of the site. The study area for this analysis includes the following intersection:

Southampton Road (Route 10/202) at North Road (signalized);

The existing conditions analysis consisted of an inventory of the traffic controls, roadway, driveway and intersection geometrics in the study area, the collection of peak hour traffic volumes, and a review of recent crash history.

## **Roadway Geometry**

Descriptions of the study area roadways and intersections are included below.

Roadways

## Southampton Road (Route 10/202)

Southampton Road (Route 10 & 202), a minor arterial roadway, is a north-south roadway that provides a connection between communities to the south and north of the project site, as well as Interstate 90 to the south. Southampton Road south of North Road is designated as Route 10 & 202, while north of North Road it is designated at Route 10. Southampton Road has a typical cross section consisting of



two travel lanes (1 lane per direction) with exclusive turning lanes at key intersections and wide shoulders. In front of the site the pavement width varies between 45 feet and 50 feet, carrying one travel lane in each direction. The posted speed limit along Southampton Road is 40 mph in the vicinity of the site. No sidewalks or pedestrian accommodations are provided along this section of Southampton Road. The abutting land uses along Southampton Road are a mix of commercial, institutional, and residential, as well as several large distribution facilities. Barnes Air National Guard Base is located off the opposite side of Southampton Road, in the vicinity of the site.

## North Road (Route 202)

North Road (Route 202) is an east-west roadway providing connection to Interstate 91 to the east. North Road is a minor collector roadway. North Road to the east of Southampton Road is designated as Route 202, while North Road to the west of Southampton Road does not carry a designation. North Road has a cross section consisting of two travel lanes (1 per direction), without shoulders adjacent to the site. The pavement width is approximately 30 feet in the vicinity of the project site. The abutting land use along North Road in the study area is predominantly residential, minor commercial and institutional. The posted speed limit is 40 mph in the vicinity of the site. No sidewalks or pedestrian accommodations are provided along North Road.

Intersections

## Southampton Road (Rte 10 & 202) at North Road (Rte 202)

North Road intersects Southampton Road from the east and west to form this fourway signalized intersection. The North Road eastbound and westbound approaches both consist of a single multi-purpose lane, however, vehicles were observed forming multiple lanes along the westbound approach. The northbound and southbound Southampton Road approaches each provide a single multi-purpose lane, however, vehicles were observed forming multiple lanes along the both of these approaches as well. The project site is located on the southwest corner of the intersection. Land uses in the vicinity of the intersection consist of a residential home on the northeast corner, 7B's Grill and Bar, a convenience store, a hair salon, and a drive-through ATM on the northwest corner, and wooded area and a large distribution center on the southeast corner. Movements at the intersection are controlled by a 2-phase actuated-uncoordinated traffic signal.



## **Traffic Volumes**

Peak hour turning movement and classification (TMC) counts were collected on a typical weekday evening from 4:00 PM to 6:00 PM and on a typical Saturday from 11:00 AM to 1:00 PM at the study area intersection on January 24, 2013 (Thursday) and January 26, 2013 (Saturday).

Based on the TMC data, the peak hours of traffic operations for the study area intersections were determined to be 4:15 PM to 5:15 PM on a typical weekday evening, and 11:30 AM to 12:30 PM on a typical Saturday midday.

Automatic traffic recorder counts were also conducted January 25<sup>th</sup> through January 26<sup>th</sup>, 2013 along Southampton Road in front of the project site. Table 1 summarizes daily traffic volume data obtained.

## Table 1 Summary of Observed Traffic Volumes

		Friday	<b>Evening Pea</b>	k Hour		Saturday Midday Peak Hour					
Location	Weekday	_	ĸ	Dir.	Saturday	-	ĸ	Dir.			
	ADT <sup>a</sup>	Volume <sup>b</sup>	Factor <sup>c</sup>	Dist. d	ADT	Volume	Factor	Dist.			
Southampton Road (south of North Road)	12,500	1,090	8.7%	58% NB	8,830	760	8.6%	51% NB			

NOTE: ATRs conducted by Innovative Data, LLC

a daily traffic expressed in vehicles per day

b peak hour volumes expressed in vehicles per hour

c percent of daily traffic that occurs during the peak hour period

d directional distribution of peak period traffic

## Seasonal Adjustment

The traffic volume data collected for this project were obtained during the month of January. To quantify the seasonal variation of traffic volumes in the area, historic traffic data available from MassDOT were reviewed. This data indicates that traffic volumes in January are typically lower than the yearly average conditions. Therefore, a seasonal adjustment of 1.02% was applied to the traffic volumes in order to provide a conservative analysis. Figure 2 illustrates the resulting 2013 Existing conditions peak period traffic volumes for the weekday evening and Saturday midday peak hours.



Neg = < 5 Vehicles

Weekday Evening Peak (Saturday Midday Peak)



Cumberland Farms Convenience StoreFigure 2Not to ScalePeak Hour Traffic Volumes - 2013 Existing<br/>Weekday Evening and Saturday Midday Peak Hours

Westfield, Massachusetts



## **Crash History**

To identify accident trends and/or roadway deficiencies in the study area, crash data for the study area intersections were obtained from MassDOT for the most recently available three-year period (2008-2010). MassDOT reports vehicle crashes with damage greater than \$1,000 or personal injury occurrences, which can give a good indication of safety along the study corridor.

The 2011 MassDOT average crash rates for signalized intersections for District 2 (the MassDOT district designation for Westfield) is 0.82. As seen in the crash summary table found in the Appendix, the signalized intersection of Southampton Road (Route 10/202) at North Road (Route 202) is above the MassDOT District 2 average crash rate values, with a value of 1.14.

In that report, the signalized intersection experienced a total of twenty two (22) <u>reported</u> accidents over the three year period. The majority of the reported accidents were angle and rear-end accidents.



# **3** Future Conditions

To determine future demands on the roadway network, existing traffic volumes in the study area were projected to the year 2018, reflecting a five year traffic-planning horizon. Traffic volumes on the roadway network under future conditions without the project (2018 No-Build) are assumed to include all existing traffic, any new traffic due to background traffic growth, and traffic related to any specific development projects expected to be completed by the horizon year. Anticipated traffic volumes from the proposed development were added to the No-Build traffic volumes to reflect conditions with the project in place (2018 Build scenario).

## **Background Traffic Growth**

Traffic growth on area roadways is a function of the expected land development, economic activity, and changes in demographics. Several methods can be used to estimate this growth. A procedure frequently employed is to estimate an annual percentage increase and apply that increase to study area traffic volumes. An alternative procedure is to identify estimated traffic generated by planned new major developments that would be expected to impact the project study area roadways. For the purpose of this assessment, both methods were utilized.

## **Historic Traffic Growth**

Many factors influence regional traffic growth including socio-economic factors such as population, employment, regional development, and dwelling unit changes. For the purpose of this study, an annual growth rate of 2-percent per year was applied to the existing traffic volumes over the 5-year forecast period. Regional traffic growth is projected by examining historical traffic volumes and other more recent traffic studies conducted within the area. The existing traffic volumes were grown by 2-percent per year to account for potential future traffic growth.



## Site-Specific Growth

Traffic volumes in the area can be affected by other nearby developments. Based on information provided by the City of Westfield it was identified that while development opportunities currently exist within the City, they are either located too far from the study area to have a significant impact, or official applications have not been filed with the City yet.

One development that has been approved by the City but has been completely constructed is the Armbrook Senior Living Center, proposed to be located further west along North Road and provide 122 living units. Construction is currently underway, with occupancy set for the spring of 2013. Since these types of developments generate minimal traffic, it can be assumed that the traffic increase is accounted for as part of the conservative 2 percent per year background growth.

It was assumed that the site specific growth associated with any other potential developments can also be accounted for as part of the historic 2 percent per year background growth. The 2018 No-Build traffic volumes are shown on Figure 3.

## **Future Roadway Conditions**

In assessing future traffic conditions, proposed roadway improvements within the study area were considered. Based on discussions with the City of Westfield, there are currently no improvement plans that would alter the roadway cross section or characteristics. One project that is currently planned is the construction of a new water and/or sewer main, but this project is not expected to impact traffic volumes or patterns in the vicinity of the site.

## **Trip Generation**

To estimate the trip-generating characteristics for the proposed development, traffic projections were derived from trip generation rates published by the Institute of Transportation Engineers (ITE) *Trip Generation*<sup>1</sup> For the proposed gas station with convenience store, it was determined that ITE trip generation rates for gas/service station with convenience store (land use code 945) were the most appropriate rates to use. Saturday daily trips were estimated using a ratio of Saturday daily to Saturday midday peak hour estimates for LUC 820 (Shopping Center) for a corresponding square footage with trip generation similar to the Saturday midday peak hour. As noted earlier, the proposed gas station will consist of 10 vehicle fueling positions. A summary of the Cumberland Farms convenience store and fueling facility trip generation is detailed in Table 2.

<sup>1</sup> <u>Trip Generation;</u> Eighth Edition; Institute of Transportation Engineers; Washington, D.C.; 2012.



Neg = < 5 Vehicles

Weekday Evening Peak (Saturday Midday Peak)



Cumberland Farms Convenience StoreFigure 3Not to ScalePeak Hour Traffic Volumes - 2018 No-Build<br/>Weekday Evening and Saturday Midday Peak Hours

Westfield, Massachusetts



In addition, not all of the net new traffic generated by the site will be new traffic on the study area roadways. Given the nature of a fueling facility, the demand is generally a function of the adjacent street traffic volumes, and typically consists of primarily drive-by traffic. Drive-by traffic is defined as vehicles already on the roadway network who decide to stop at the fueling facility prior to proceeding to their original destination. ITE data suggests that approximately 62 percent of the traffic generated by a gas station with convenience store could be pass-by traffic. However, to be consistent with EOEA/EOT Guidelines for Traffic Impact Assessments and to provide a conservative analysis, only 25 percent of the traffic generated by the site was assumed to be pass-by trips. The resulting trip generation is presented in Table 2.

Table 2	
Site Generated	<b>Traffic Summary</b>

Time Period	Future <sup>1</sup> (16 vfp)	Pass-By Trips <sup>2</sup>	Total Site Trips
Weekday Dailyª	1,630	410	1,220
Weekday Evening Peak Hourb			
Enter	70	20	50
<u>Exit</u>	<u>65</u>	<u>15</u>	<u>50</u>
Total	135	35	100
Saturday Daily <sup>a</sup>	1,820	460	1,360
Saturday Midday Peak Hour <sup>b</sup>			
Enter	90	25	65
<u>Exit</u>	<u>85</u>	<u>20</u>	<u>65</u>
Total	175	45	130

Source: Trip Generation, 8th Edition; Institute of Transportation Engineers (ITE); Washington, D.C. (2008).

Note: numbers rounded to the nearest 5.

vehicles per day а b

1 2 vehicles per hour

Trip generation based on LUC 945 (Gas/Service Station w/Convenience Store) for 10 vehicle fueling positions.

Represents a conservative 25% pass-by rate.

As shown in Table 2, the site is not expected to generate a significant amount of trips during the peak hours. To put the amount of site generated traffic into perspective, the 50 new trips during the weekday evening peak hour is less than 1 new vehicle entering the site per minute.



## **Trip Distribution and Assignment**

The regional trip distribution of site generated traffic due to the proposed development is expected to reflect the vehicle patterns of existing vehicle trips accessing the site. Table 3 illustrates the trip distribution along the study area approaches.

## Table 3 Vehicle Trip Distribution Summary

Direction (To/From)	Travel Route	New Site-Generated Traffic Weekday Evening Peak Hour	New Site-Generated Traffic Saturday Midday Peak Hour
East	North Road (Route 202)	33%	22%
West	North Road	7%	13%
North	Southampton Road (Route 10)	18%	26%
<u>South</u>	Southampton Road (Route 10/202)	<u>42%</u>	<u>39%</u>
Total	All Routes	100%	100%

As illustrated in Table 3, the majority of site generated traffic is expected to approach the site from the south on Southampton Road (Route 10/202). This accounts for approximately 42 percent and 39 percent of the peak hour traffic during the weekday evening and Saturday midday peak hours, respectively. Using these assumptions and the distribution of traffic to/from the site; traffic was assigned to the driveways.

By using the existing traffic volumes, the anticipated Trip Generation Increase numbers from Table 2, and the trip distribution percentages, the anticipated increase in traffic volumes along each leg of the surrounding roadway network can be estimated. For example, on a daily basis, Southampton Road (Route 10/202) carries approximately 12,500 vehicles per day south of North Road. The trip distribution exercise that was done shows that approximately 42% of site traffic comes from and returns to the south along Southampton Road during the weekday evening peak hour. The total estimated daily increase in traffic volumes is 1,220 as shown in Table 2. From this information, it can be calculated that Southampton Road is estimated to carry approximately 510 (42% of 1,220 total vehicles per day) more vehicles per day, representing only a 4% increase over existing conditions.

During the weekday evening peak hour, Southampton Road (Route 10/202) south of North Road currently carries 1,090 vehicles per hour (approximately 18 vehicles every minute). The total trips during the weekday evening peak hour that this site is proposed to generate is approximately 100 trips per hour (from Table 2). Of the 100 new trips per hour, approximately 42 (42% of 100) will travel along Southampton Road (Route 10/202) south of North Road, which represents a minimal increase of less than 1 new vehicle per minute.



## Site Driveways and Circulation

As currently proposed, the Cumberland Farms convenience store and fueling facility will be adequately served by three site driveways, one full access driveway on Southampton Road (Route 10/202) and one full access driveway on North Road, as well as an entrance only driveway along Southampton Road located closer to the signalized intersection of Southampton Road (Route 10/202) at North Road (Route 202). The two new full-access driveways will be located further away from the signalized intersection to help avoid conflicts with traffic at the intersection.

The proposed *West Site Driveway* intersects North Road from the south to form an unsignalized intersection. North Road is proposed to continue operating freely, while the site driveway approach is to operate under "STOP" control. The driveway approach will provide a shared right/left turn lane. The proposed site driveway is located approximately 115 feet west of the signalized intersection.

The proposed *South Site Driveway* intersects Southampton Road (Route 10/202) from the west and forms a three-legged unsignalized intersection. Southampton Road is proposed to continue operating freely, while the site driveway approach is to operate under "STOP" control. The driveway approach will provide a shared right/left turn lane. This proposed site driveway is located approximately 225 feet south of the signalized intersection.

The proposed *North Site Driveway* intersects Southampton Road (Route 10/202) from the west and forms a three-legged unsignalized intersection. Southampton Road is proposed to continue operating freely, while the site driveway is an entrance only driveway, not allowing vehicles to exit. This proposed site driveway is located approximately 50 feet south of the signalized intersection.

The location of the site driveways allow for full use of the site from a vehicle circulation perspective. At fueling facilities it is ideal to allow multiple access and egress points so that traffic does not become congested on site. If vehicles are allowed to access the site and pull into a site driveway without conflict, it minimizes the chances of impacting the adjacent roadways.

## **Build Traffic Volumes**

Design year 2018 Build traffic volumes for study area roadways were determined by estimating site-generated traffic volumes and distributing these volumes over the study area roadways. These site-generated volumes were added to the 2018 No-Build traffic volumes to create the year 2018 Build traffic volume networks. The 2018 Build weekday evening and Saturday midday peak hour traffic volumes are illustrated on Figures 4 and 5, respectively.



# Not to Scale

Cumberland Farms Convenience Store and Fueling Facility

e Store

Figure 4

Peak Hour Traffic Volumes 2018 Build Weekday Evening Peak Hour Westfield, Massachusetts



# Not to Scale

Cumberland Farms Convenience Store and Fueling Facility

Peak Hour Traffic Volumes

Figure 5

Peak Hour Traffic Volumes 2018 Build Saturday Midday Peak Hour Westfield, Massachusetts



# **Traffic Operations Analysis**

Measuring existing traffic volumes and projecting future traffic volumes quantifies traffic flow within the study area. To assess quality of flow, roadway capacity analyses were conducted with respect to Existing, projected No-Build, and Build traffic volume conditions. Capacity analyses provide an indication of how well the roadway facilities serve the traffic demands placed upon them. Roadway operating conditions are classified by calculated levels of service.

## Level-Of-Service Criteria

The evaluation criteria used to analyze area intersections in this traffic study are based on the 2000 Highway Capacity Manual (HCM)<sup>2</sup>. The term 'Level of service' (LOS) is used to denote the different operating conditions that occur on a given roadway segment under various traffic volume loads. It is a qualitative measure that considers a number of factors including roadway geometry, speed, travel delay and freedom to maneuver. Level of service provides an index to the operational qualities of a roadway segment or an intersection. Level-of-service designations range from A to F, with LOS A representing the best operating conditions and LOS F representing the worst operating conditions.

In addition to LOS, two other measures of effectiveness (MOEs) are typically used to quantify the traffic operations at intersections; volume-to-capacity ratio (v/c) and delay (expressed in seconds per vehicle). For example, an existing v/c ratio of 0.9 for an intersection indicates that the intersection is operating at 90 percent of its available capacity. A delay of 15 seconds for a particular vehicular movement or approach indicates that vehicles on the movement or approach will experience an average additional travel time of 15 seconds. It should be noted that v/c and delay could have a range of values for a given LOS letter designation. Comparison of intersection capacity results therefore requires that, in addition to the LOS, the other MOEs should also be considered.

The level-of-service designations, which are based on delay, are reported differently for signalized and unsignalized intersections. For signalized intersections, the analysis considers the operation of all traffic entering the intersection and the

♦ 2

Transportation Research Board, Highway Capacity Manual, Washington, D.C., 2000.



LOS designation is for overall conditions at the intersection. For unsignalized intersections, however, the analysis assumes that traffic on the mainline is not affected by traffic on the side streets. Thus, the LOS designation is for the critical movement exiting the side street, which is generally the left turn out of the side street or site driveway. Table 4 shows the level of service criteria for both signalized intersections and unsignalized intersections.

It should be noted that the analytical methodologies typically used for the analysis of unsignalized intersections use conservative analysis parameters, such as long critical gaps. Actual field observations indicate that drivers on minor streets generally accept shorter gaps in traffic than those used in the analysis procedures and therefore experience less delay than reported by the analysis software. The analysis methodologies also do not fully take into account the beneficial grouping effects caused by nearby signalized intersections. The net effect of these analysis procedures is the over-estimation of calculated delays at unsignalized intersections in the study area. Cautious judgment should therefore be exercised when interpreting the capacity analysis results at unsignalized intersections.

## Table 4 Level of Service Criteria

Level of Service	Signalized Intersection	Unsignalized Intersection
A	0 to 10 seconds	0 to 10 seconds
В	10 to 20 seconds	10 to 15 seconds
С	20 to 35 seconds	15 to 25 seconds
D	35 to 55 seconds	25 to 35 seconds
E	55 to 80 seconds	35 to 50 seconds
F	Greater than 80 seconds	Greater than 50 seconds

Source: 2000 Highway Capacity Manual Exhibits 16-2 and 17-2



## Signalized Intersections Capacity Analysis

Capacity analyses conducted for the signalized intersections are summarized in Table 5. The capacity analyses were conducted for 2013 Existing, 2018 No-Build and 2018 Build conditions.

## Table 5 Signalized Intersection Capacity Analysis Summary

			2013 Existin	g	<u>2</u>	018 No-Bui	ld	2018 Build			
Location	Peak Hour	<b>v/c</b> <sup>1</sup>	Delay <sup>2</sup>	LOS <sup>3</sup>	v/c	Delay	LOS	v/c	Delay	LOS	
Southampton Road (Route 10/202)	Weekday Evening	0.81	17.6	В	0.90	23.5	С	0.93	27.1	С	
at North Road (Route 202)*	Saturday Midday	0.53	8.7	А	0.59	9.7	А	0.61	10.4	В	

volume to capacity ratio

average delay in seconds per vehicle level of service

3

2

the westbound approach was modeled as it operates in the field with two approach lanes

The signalized capacity analysis summary in Table 5 indicates that the signalized intersection of Southampton Road (Route 10/202) at North Road (Route 202) is not expected to deteriorate in LOS from the No-Build to the Build conditions during the weekday evening peak hour. Furthermore, the intersection is expected to operate at acceptable levels of service during the Build conditions, with slight increases in delay.

## **Unsignalized Intersection Capacity Analysis**

Three unsignalized site driveways were analyzed for the 2018 Build conditions. The results of the analyses are shown in Table 6.

Table 6 shows that during the 2018 Build conditions the two full access site driveways are expected to operate at an acceptable LOS during both the peak hours.



## Table 6 Unsignalized Intersection Capacity Analysis Summary

		lane		2018 N	lo-Build			2018 Build							
Location	Period	Group	Dem <sup>1</sup>	v/c²	Delay <sup>3</sup>	LOS⁴	Dem	v/c	Delay	LOS					
South Site Drive (Site Drive 1) at Southampton Road	Weekday Evening	EB		1	NA		45	0.19	21.9	С					
	Saturday Midday	EB		1	NA		50	0.13	15.3	С					
North Site Drive	Weekday Evening	NB		1	NA		5	0.01	0.1	A					
Southampton Road	Saturday Midday	NB		1	NA		10	0.01	0.3	A					
West Site Drive	Weekday Evening	NB		1	NA		20	0.03	10.2	В					
North Road	Saturday Midday	NB		1	NA		35	0.05	10.0	A					

demand in vehicles per hour volume to capacity ratio delay, measured in seconds per vehicle

 1
 demand in vehicles per hour

 2
 volume to capacity ratio

 3
 delay, measured in seconds per vehicle

 4
 level of service

 NA
 driveways do not exist during No-Build scenario



# **5** Conclusions

This study has been prepared to evaluate the traffic impacts associated with the construction of a proposed Cumberland Farms Convenience Store with Gasoline Sales (10 vehicle fueling positions) to be located on the southwestern corner of the intersection of Southampton Road (Route 10/202) at North Road (route 202) in the City of Westfield, Massachusetts. The following is a summary of study findings:

- The proposed redevelopment is expected to generate approximately 135 (70 enter, 65 exit) total vehicle trips during the weekday afternoon peak hour, and 175 (90 enter, 85 exit) total vehicle trips during the Saturday midday peak hour. Given the nature of a fueling facility, the demand is generally a function of the adjacent street traffic volumes, and typically consists of primarily drive-by traffic. For this type of development, approximately 62 percent of the site-generated traffic could be drive-by traffic or traffic that is already on the roadway. However, because the project abuts State Highway, traffic guidelines set by the State and MassDOT only allow a 25 percent pass-by credit when conducting a traffic study. Therefore, this traffic study utilized a conservative methodology.
- The Cumberland Farms convenience store and fueling facility will be adequately served by three site driveways, one full access driveway on Southampton Road (Route 10/202) and one full access driveway on North Road, as well as an entrance only driveway along Southampton Road. The location of the site driveways allow for full use of the site from a vehicle circulation perspective. At fueling facilities it is ideal to allow multiple access points so that traffic does not impact the adjacent roadways, and so that traffic can circulate the site in a more efficient manner.
- The results of this study (as shown in Tables 5 and 6) indicate that the study area intersection and roadways are not expected to be significantly impacted by the proposed project, and there is sufficient capacity to accommodate the conservative increase in traffic that has been projected.

In summary, it is the finding of this traffic impact and access study is that the study area intersections and roadways are not expected to be significantly impacted by the addition of the anticipated traffic generated by the proposed development.

# **Traffic Appendix**

## > Observed Traffic Volume Data

- Intersection Counts (PM & SAT Peak Hours)
- Automatic Traffic Recorder (ATR) Data

## > ITE Trip Generation Calculations

- LUC 945 "Gasoline/Service Station with Convenience Market"
- VHB Calculations

## Crash Data

- o 2008-2010 Crash Summary
- Crash Rate Worksheet

## > Operational Analyses

- o Intersection Capacity Analysis
- Cumberland Farms Concept Plan

# Observed Traffic Volume Data Intersection Counts

ATR Counts



Belchertown, Massachusetts www.innovativedatallc.com or 1.413.668.5094

N / S: Southampton Road E / W: North Road City, State: Westfield, Massachusetts Client: VHB / J. Locke

File Name : PM Peak - Southampton @ North Site Code : 1 Start Date : 1/24/2013 Page No : 1

						Group	os Prir	nted- F	PCs ar	nd Peds	<u>s - Hea</u>	avy Ve	hicles	- Bicy	/cles							
		So	utham	pton			North					Southampton					North					
		Fr	rom No	orth			From East					Fr	om So	outh								
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total	
04:00 PM	2	46	22	0	70	31	31	80	0	142	96	44	10	0	150	7	12	1	0	20	382	
04:15 PM	4	61	15	0	80	24	32	46	0	102	76	52	3	0	131	10	21	6	0	37	350	
04:30 PM	4	40	18	0	62	37	35	58	0	130	66	77	8	0	151	7	17	5	0	29	372	
04:45 PM	3	57	10	0	70	39	48	40	0	127	83	73	10	0	166	7	19	4	0	30	393	
Total	13	204	65	0	282	131	146	224	0	501	321	246	31	0	598	31	69	16	0	116	1497	
05:00 PM	5	47	18	0	70	52	39	47	0	138	85	94	11	0	190	6	13	1	0	20	418	
05:15 PM	6	44	15	0	65	35	38	46	0	119	53	64	12	0	129	7	22	6	0	35	348	
05:30 PM	4	42	10	0	56	32	42	44	0	118	39	52	3	0	94	12	32	6	0	50	318	
05:45 PM	2	39	14	0	55	39	22	30	0	91	48	39	7	0	94	6	14	2	0	22	262	
Total	17	172	57	0	246	158	141	167	0	466	225	249	33	0	507	31	81	15	0	127	1346	
Grand Total	30	376	122	0	528	289	287	391	0	967	546	495	64	0	1105	62	150	31	0	243	2843	
Apprch %	5.7	71.2	23.1	0		29.9	29.7	40.4	0		49.4	44.8	5.8	0		25.5	61.7	12.8	0			
Total %	1.1	13.2	4.3	0	18.6	10.2	10.1	13.8	0	34	19.2	17.4	2.3	0	38.9	2.2	5.3	1.1	0	8.5		
PCs and Peds																						
% PCs and Peds	93.3	98.1	98.4	0	97.9	98.3	97.2	92.6	0	95.7	97.4	98.6	98.4	0	98	96.8	94.7	96.8	0	95.5	97	
Heavy Vehicles																						
% Heavy Vehicles	6.7	1.9	1.6	0	2.1	1.7	2.8	7.4	0	4.3	2.6	1.4	1.6	0	2	3.2	5.3	3.2	0	4.5	3	
Bicycles	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
% Bicycles	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	

	Southampton North								Southampton						North						
		F	rom No	orth			F	rom E	ast			From South					From West				
Start Time	Right	Thru		Peds	App. Total	Right	Thru		Peds	App. Total	Right	Thru		Peds	App. Total	Right	Thru		Peds	App. Total	Int. Total
Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1																					
Peak Hour for	or Enti	re Inte	rsectio	n Beg	ins at 04	4:15 P	М														
04:15 PM	4	61	15	0	80	24	32	46	0	102	76	52	3	0	131	10	21	6	0	37	350
04:30 PM	4	40	18	0	62	37	35	58	0	130	66	77	8	0	151	7	17	5	0	29	372
04:45 PM	3	57	10	0	70	39	48	40	0	127	83	73	10	0	166	7	19	4	0	30	393
05:00 PM	5	47	18	0	70	52	39	47	0	138	85	94	11	0	190	6	13	1	0	20	418
Total Volume	16	205	61	0	282	152	154	191	0	497	310	296	32	0	638	30	70	16	0	116	1533
% App. Total	5.7	72.7	21.6	0		30.6	31	38.4	0		48.6	46.4	5	0		25.9	60.3	13.8	0		
PHF	.800	.840	.847	.000	.881	.731	.802	.823	.000	.900	.912	.787	.727	.000	.839	.750	.833	.667	.000	.784	.917



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N / S: Southampton Road E / W: North Road City, State: Westfield, Massachusetts Client: VHB / J. Locke File Name : PM Peak - Southampton @ North Site Code : 1 Start Date : 1/24/2013 Page No : 1

								Gro	ups Pr	inted- I	leavy	Vehic	les								_
		So	utham	pton				North	່		-	So	utham	pton				Nortl	n		
		Fr	om N	orth			F	rom E	ast			Fr	om So	buth			Fr	om W	/est		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
04:00 PM	0	2	0	0	2	0	2	4	0	6	1	1	0	0	2	1	2	0	0	3	13
04:15 PM	0	1	0	0	1	1	1	4	0	6	5	0	0	0	5	1	1	1	0	3	15
04:30 PM	0	0	0	0	0	0	3	6	0	9	1	1	1	0	3	0	0	0	0	0	12
04:45 PM	0	1	1	0	2	1	0	3	0	4	3	1	0	0	4	0	0	0	0	0	10
Total	0	4	1	0	5	2	6	17	0	25	10	3	1	0	14	2	3	1	0	6	50
05:00 PM	0	0	0	0	0	0	0	4	0	4	1	2	0	0	3	0	0	0	0	0	7
05:15 PM	1	0	0	0	1	0	1	3	0	4	2	1	0	0	3	0	1	0	0	1	9
05:30 PM	1	0	1	0	2	2	1	3	0	6	1	1	0	0	2	0	3	0	0	3	13
05:45 PM	0	3	0	0	3	1	0	2	0	3	0	0	0	0	0	0	1	0	0	1	7
Total	2	3	1	0	6	3	2	12	0	17	4	4	0	0	8	0	5	0	0	5	36
Grand Total	2	7	2	0	11	5	8	29	0	42	14	7	1	0	22	2	8	1	0	11	86
Apprch %	18.2	63.6	18.2	0		11.9	19	69	0		63.6	31.8	4.5	0		18.2	72.7	9.1	0		
Total %	2.3	8.1	2.3	0	12.8	5.8	9.3	33.7	0	48.8	16.3	8.1	1.2	0	25.6	2.3	9.3	1.2	0	12.8	

		So	utham	oton				North	ı			So	utham	pton				North	ı		
		Fr	rom No	orth			F	rom E	ast			Fi	rom So	buth			F	rom W	est		1
Start Time	Right	Thru		Peds	App. Total	Right	Thru		Peds	App. Total	Right	Thru		Peds	App. Total	Right	Thru		Peds	App. Total	Int. Total
Peak Hour A	nalysi	s From	n 04:00	) PM t	o 05:45	PM - F	Peak 1	of 1													
Peak Hour for	or Entii	re Inte	rsectio	n Beg	ins at 04	4:00 P	M														
04:00 PM	0	2	0	0 Ŭ	2	0	2	4	0	6	1	1	0	0	2	1	2	0	0	3	13
04:15 PM	0	1	0	0	1	1	1	4	0	6	5	0	0	0	5	1	1	1	0	3	15
04:30 PM	0	0	0	0	0	0	3	6	0	9	1	1	1	0	3	0	0	0	0	0	12
04:45 PM	0	1	1	0	2	1	0	3	0	4	3	1	0	0	4	0	0	0	0	0	10
Total Volume	0	4	1	0	5	2	6	17	0	25	10	3	1	0	14	2	3	1	0	6	50
% App. Total	0	80	20	0		8	24	68	0		71.4	21.4	7.1	0		33.3	50	16.7	0		
PHF	.000	.500	.250	.000	.625	.500	.500	.708	.000	.694	.500	.750	.250	.000	.700	.500	.375	.250	.000	.500	.833



Belchertown, Massachusetts www.innovativedatallc.com or 1.413.668.5094

N / S: Southampton Road E / W: North Road City, State: Westfield, Massachusetts Client: VHB / J. Locke

File Name : Sat Peak - Southampton @ North Site Code : 1 Start Date : 1/26/2013 Page No : 1

						Group	os Prir	nted- F	PCs ar	nd Peds	<u>- Hea</u>	ivy Ve	hicles	- Bicy	cles						
		So	utham	pton				North	ו			So	utham	pton				North	ו		
		Fr	om No	orth			F	rom E	ast			Fr	om So	outh			Fr	om W	/est		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
11:00 AM	2	43	21	0	66	23	14	30	0	67	52	29	5	0	86	3	14	2	0	19	238
11:15 AM	3	45	26	0	74	15	22	26	0	63	41	43	5	0	89	1	10	3	0	14	240
11:30 AM	1	43	27	0	71	12	13	28	0	53	57	48	8	0	113	11	25	2	0	38	275
11:45 AM	1	47	25	0	73	22	13	34	0	69	48	31	7	0	86	9	24	4	0	37	265
Total	7	178	99	0	284	72	62	118	0	252	198	151	25	0	374	24	73	11	0	108	1018
12:00 PM	5	38	27	0	70	13	7	32	0	52	64	44	6	0	114	6	20	3	0	29	265
12:15 PM	2	41	25	0	68	18	17	42	0	77	53	56	7	0	116	5	38	2	0	45	306
12:30 PM	1	33	25	0	59	21	15	28	0	64	54	34	3	0	91	7	24	3	0	34	248
12:45 PM	1	42	20	0	63	15	13	32	0	60	47	40	3	0	90	5	18	1	0	24	237
Total	9	154	97	0	260	67	52	134	0	253	218	174	19	0	411	23	100	9	0	132	1056
Grand Total	16	332	196	0	544	139	114	252	0	505	416	325	44	0	785	47	173	20	0	240	2074
Apprch %	2.9	61	36	0		27.5	22.6	49.9	0		53	41.4	5.6	0		19.6	72.1	8.3	0		
Total %	0.8	16	9.5	0	26.2	6.7	5.5	12.2	0	24.3	20.1	15.7	2.1	0	37.8	2.3	8.3	1	0	11.6	
PCs and Peds																					
% PCs and Peds	87.5	99.4	98	0	98.5	98.6	97.4	94.8	0	96.4	98.3	99.4	93.2	0	98.5	100	100	95	0	99.6	98.1
Heavy Vehicles																					
% Heavy Vehicles	12.5	0.6	2	0	1.5	1.4	2.6	5.2	0	3.6	1.7	0.6	6.8	0	1.5	0	0	5	0	0.4	1.9
Bicycles	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
% Bicycles	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

		So	utham	pton				North	1			So	utham	pton				North	ı		
		Fi	rom No	orth			F	rom Ea	ast			Fi	om Sc	outh			F	rom W	est		
Start Time	Right	Thru		Peds	App. Total	Right	Thru		Peds	App. Total	Right	Thru		Peds	App. Total	Right	Thru		Peds	App. Total	Int. Total
Peak Hour A	nalysi	s From	n 11:00	O AM t	o 12:45	PM - F	Peak 1	of 1													
Peak Hour for	or Enti	re Inte	rsectio	n Beq	ins at 1	1:30 A	M														
11:30 AM	1	43	27	Õ	71	12	13	28	0	53	57	48	8	0	113	11	25	2	0	38	275
11:45 AM	1	47	25	0	73	22	13	34	0	69	48	31	7	0	86	9	24	4	0	37	265
12:00 PM	5	38	27	0	70	13	7	32	0	52	64	44	6	0	114	6	20	3	0	29	265
12:15 PM	2	41	25	0	68	18	17	42	0	77	53	56	7	0	116	5	38	2	0	45	306
Total Volume	9	169	104	0	282	65	50	136	0	251	222	179	28	0	429	31	107	11	0	149	1111
% App. Total	3.2	59.9	36.9	0		25.9	19.9	54.2	0		51.7	41.7	6.5	0		20.8	71.8	7.4	0		
PHF	.450	.899	.963	.000	.966	.739	.735	.810	.000	.815	.867	.799	.875	.000	.925	.705	.704	.688	.000	.828	.908



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N / S: Southampton Road E / W: North Road City, State: Westfield, Massachusetts Client: VHB / J. Locke File Name : Sat Peak - Southampton @ North Site Code : 1 Start Date : 1/26/2013 Page No : 1

								Grou	ups Pr	inted- H	leavy	Vehic	les								_
		So	utham	pton				North	່		-	So	utham	pton				North	ו		1
		Fr	om N	orth			F	rom E	ast			<u> </u>	om So	outh			Fr	om W	est		
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
11:00 AM	0	0	0	0	0	1	0	2	0	3	1	0	1	0	2	0	0	0	0	0	5
11:15 AM	1	0	2	0	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3
11:30 AM	1	0	2	0	3	0	0	1	0	1	1	0	0	0	1	0	0	0	0	0	5
11:45 AM	0	1	0	0	1	0	0	2	0	2	0	0	0	0	0	0	0	0	0	0	3
Total	2	1	4	0	7	1	0	5	0	6	2	0	1	0	3	0	0	0	0	0	16
12:00 PM	0	0	0	0	0	0	0	0	0	0	2	0	0	0	2	0	0	1	0	1	3
12:15 PM	0	1	0	0	1	0	2	2	0	4	0	0	1	0	1	0	0	0	0	0	6
12:30 PM	0	0	0	0	0	0	0	1	0	1	2	0	0	0	2	0	0	0	0	0	3
12:45 PM	0	0	0	0	0	1	1	5	0	7	1	2	1	0	4	0	0	0	0	0	11
Total	0	1	0	0	1	1	3	8	0	12	5	2	2	0	9	0	0	1	0	1	23
Grand Total	2	2	4	0	8	2	3	13	0	18	7	2	3	0	12	0	0	1	0	1	39
Apprch %	25	25	50	0		11.1	16.7	72.2	0		58.3	16.7	25	0		0	0	100	0		
Total %	5.1	5.1	10.3	0	20.5	5.1	7.7	33.3	0	46.2	17.9	5.1	7.7	0	30.8	0	0	2.6	0	2.6	

		So	utham	pton				North	I			Sc	utham	pton				North	1		
		Fi	rom No	orth			F	rom E	ast			F	rom Sc	outh			F	rom W	est		1
Start Time	Right	Thru		Peds	App. Total	Right	Thru		Peds	App. Total	Right	Thru		Peds	App. Total	Right	Thru		Peds	App. Total	Int. Total
Peak Hour A	Analysi	s From	n 11:00	) AM to	o 12:45	PM - F	Peak 1	of 1													
Peak Hour for	or Enti	re Inte	rsectio	n Beg	ins at 12	2:00 P	М														
12:00 PM	0	0	0	Õ	0	0	0	0	0	0	2	0	0	0	2	0	0	1	0	1	3
12:15 PM	0	1	0	0	1	0	2	2	0	4	0	0	1	0	1	0	0	0	0	0	6
12:30 PM	0	0	0	0	0	0	0	1	0	1	2	0	0	0	2	0	0	0	0	0	3
12:45 PM	0	0	0	0	0	1	1	5	0	7	1	2	1	0	4	0	0	0	0	0	11
Total Volume	0	1	0	0	1	1	3	8	0	12	5	2	2	0	9	0	0	1	0	1	23
% App. Total	0	100	0	0		8.3	25	66.7	0		55.6	22.2	22.2	0		0	0	100	0		
PHF	.000	.250	.000	.000	.250	.250	.375	.400	.000	.429	.625	.250	.500	.000	.563	.000	.000	.250	.000	.250	.523

## Innovative Data, LLC

Location: Southampton Road Location: South of North Road Location: Westfield, Massachusetts Client: VHB / J. Locke

## PO Box 468 Belchertown, Massachusetts innovativedatallc.com or 1.413.668.5094

Time         Fri         A.M.         P.M.         A.M.         P.M.         Sat         A.M.         P.M.         A.M.         P.M.         Sat         A.M.         P.M.         A.	Start	01-Feb-13	Nort	hbound	Sout	thbound	Cor	nbined	02-Feb-	Nor	hbound	Sou	thbound	Con	nbined
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	Time	Fri	A.M.	P.M.	A.M.	P.M.	A.M.	P.M.	Sat	A.M.	P.M.	A.M.	P.M.	A.M.	P.M.
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	12:00		20	112	9	89	29	201		23	114	17	80	40	194
12:30       24       106       3       102       27       206       10       72       14       80       24       126         12:45       10       15       88       6       94       21       182       25       88       8       87       33       173         01:15       14       88       90       6       92       12       182       11       90       5       84       16       176         01:15       14       88       90       16       87       208       12       92       14       80       26       172         02:00       10       106       8       102       18       208       8       77       74       13       78       20       152         02:15       3       128       4       106       7       224       7       74       13       78       20       152         03:15       3       128       4       96       7       222       4       80       4       108       24       116       12       144       117       20       22       14       80       4       108       16	12:15		21	94	4	112	25	206		23	102	14	75	37	177
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	12:30		24	106	3	102	27	208		10	72	14	80	24	152
01:00         15         88         6         94         21         182         25         88         97         33         173           01:15         14         88         90         6         92         12         182         11         96         5         84         16         180           01:46         1         119         6         89         7         208         12         92         14         80         5         84         16         180           02:15         3         128         4         106         7         234         7         74         13         78         20         152           02:30         8         136         7         112         15         248         5         72         7         152           03:35         3         14         147         12         305         3         95         5         72         8         107           03:45         5         164         8         94         13         248         2         76         6         98         8         117           03:45         5         154         8	12:45		10	106	14	98	24	204		10	88	6	83	16	171
11:15       14       14       8       5       96       19       184       7       88       9       00       16       172         01:30       6       99       6       92       12       162       11       96       5       84       16       172         02:00       10       106       8       106       7       224       7       74       13       76       22       14         02:00       10       106       8       106       7       224       7       74       13       76       22       149         02:15       3       128       4       106       7       224       4       96       7       12       300       16       772       7       152         03:30       4       764       96       7       222       4       80       4       82       8       16       16       16       172       16       98       8       174         03:30       4       764       7       8       9       16       77       3       16       172       16       16       173       22       8       3 <t< td=""><td>01.00</td><td></td><td>15</td><td>88</td><td>6</td><td>94</td><td>21</td><td>182</td><td></td><td>25</td><td>86</td><td>8</td><td>87</td><td>33</td><td>173</td></t<>	01.00		15	88	6	94	21	182		25	86	8	87	33	173
	01.15		14	88	5	96	19	184		7	88	9	90	16	178
0146         1         119         6         89         7         208         12         20         14         80         22         14           02:00         10         106         8         102         18         208         8         87         13         62         21         149           02:15         3         128         4         106         7         224         7         13         78         20         152           02:30         8         136         7         12         5248         5         96         4         108         9         240           03:00         15         12         4         98         97         222         4         80         4         82         8         167           03:30         4         164         3         112         230         3         95         5         72         8         105         13         163         12         18         163         12         148         2         76         6         98         8         174         13         144         144         14         10         73         18         167	01:30		6	90	6	92	12	182		11	96	5	84	16	180
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	01:45		1	119	6	89	7	208		12	92	14	80	26	172
02:15         3         122         4         106         7         234         7         74         13         78         20         152           02:30         8         136         7         112         15         246         5         96         4         108         9         204           02:45         4         101         4         117         8         227         8         902         2         70         10         162           03:30         4         166         8         141         12         305         3         95         5         72         8         106         13         248         2         76         6         98         8         17           04:15         6         172         16         13         282         286         2         94         7         70         9         164           04:15         6         172         18         106         33         224         8         94         10         73         18         107           05:00         15         167         18         106         33         224         4         83	02:00		10	106	8	102	18	208		8	87	13	62	21	149
02:30         8         136         7         112         15         248         5         96         4         108         9         20           03:45         3         126         4         96         7         122         4         80         4         96         7         222         4         80         4         86         8         126         303         3         4         96         7         222         4         80         4         86         8         182         8         182         8         182         8         182         8         182         8         182         8         182         18         18         18         18         18         13         185         14         277         1         7         18         18         18         18         18         18         18         18         18         18         18         18         18         18         18         18         18         14         12         18         19         11         12         18         12         18         14         12         16         12         18         14         13         12	02:15		3	128	4	106	7	234		7	74	13	78	20	152
0245         4         110         4         117         8         227         8         902         2         700         10         152           03:15         3         126         4         96         7         222         4         80         4         82         8         162           03:30         4         966         8         141         12         305         3         95         5         7         7         152           03:30         4         966         7         222         260         2         76         6         93         8         164           04:00         6         172         17         178         2         81         16         12         18         16         12         18         16         12         18         16         12         18         17         10         18         16         19         16         17         16         18         14         13         12         146           04:45         10         10         34         12         16         17         16         73         12         146         13         12	02:30		8	136	7	112	15	248		5	96	4	108	9	204
03:00         15         142         4         68         19         240         2         80         5         72         7         152           03:30         4         164         8         141         12         305         5         72         8         167           03:45         5         154         8         94         13         248         2         76         6         98         8         177           03:45         5         154         8         94         13         248         2         94         7         70         9         184           04:0         6         152         16         177         22         289         2         94         7         70         9         184           04:15         6         152         18         106         33         2244         8         94         10         73         18         167           05:00         15         167         18         106         33         224         4         433         9         41         13         124           05:0         166         66         18         64 <td>02:45</td> <td></td> <td>4</td> <td>110</td> <td>4</td> <td>117</td> <td>8</td> <td>227</td> <td></td> <td>8</td> <td>92</td> <td>2</td> <td>70</td> <td>10</td> <td>162</td>	02:45		4	110	4	117	8	227		8	92	2	70	10	162
03:15         3         126         4         96         7         222         4         80         4         82         8         162           03:30         4         164         8         111         2005         3         95         5         72         2         8         107           03:45         5         154         8         94         13         246         2         76         6         98         8         174           04:00         6         172         18         105         14         22         266         2         44         7         70         9         164           04:30         12         18         16         117         22         266         2         44         7         70         9         164           04:30         12         18         16         137         12         144         10         11         13         124         144         13         124         144         13         124         144         13         127         16         72         255         144         13         127         144         127         144         1	03.00		15	142	4	98	19	240		2	80	5	72	7	152
03:30         4         1764         8         147         12         305         3         55         5         72         8         167           03:45         5         152         8         105         14         2277         1         78         2         81         3         159           04:15         6         152         16         117         22         269         2         94         7         70         9         164           04:45         16         152         18         106         33         2264         8         94         10         73         18         167           05:00         15         167         18         106         33         2244         8         94         10         73         18         167           05:00         15         17         153         35         92         52         245         4         83         9         41         13         124           05:00         16         66         18         64         34         130         127         168         111         199         16         74         22         58	03:15		3	126	4	96	7	222		4	80	4	82	. 8	162
03:345         5         754         8         94         13         246         2         76         6         98         8         174           04:00         6         172         18         105         14         277         1         78         2         81         3         159           04:15         6         152         16         117         22         269         2         94         7         70         9         164           04:30         12         138         16         106         33         273         10         104         11         70         21         174           05:30         29         130         48         120         77         250         16         66         18         64         34         130           05:45         30         102         96         85         126         187         10         73         32         54         42         127         06         32         54         44         131         149         63         38         64         57         127           06:00         42         111         114         58	03:30		4	164	8	141	12	305		3	95	5	72	8	167
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	03:45		5	154	8	94	13	248		2	76	6	98	8	174
04:15         6         152         16         117         22         269         2         94         7         70         9         164           04:30         12         138         16         123         28         261         6         83         6         63         12         146           04:35         16         158         167         18         106         33         273         10         104         11         70         21         174           05:30         29         130         48         120         77         250         16         666         18         64         34         130           05:45         30         102         96         85         126         167         10         73         32         54         42         127         06:45         33         38         64         57         127         06:45         33         38         64         57         127         06:45         33         38         64         57         127         06:45         111         24         44         45         32         78         56         126         07         133         <	04.00		6	172	8	105	14	277		1	78	2	81	3	159
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	04:15		6	152	16	117	22	269		2	94	7	70	Ğ	164
04.35         16         126         13         224         8         94         10         73         18         167           05.00         15         167         18         106         33         273         10         104         11         70         21         174           05:15         17         153         35         92         52         245         4         83         9         41         13         124           05:30         29         130         48         120         77         250         16         66         18         64         34         130           06:45         30         102         96         85         126         187         10         73         18         132           06:00         42         111         69         85         126         187         10         73         134         134         134         103         114         104         134         172         188         122         148         196         63         38         64         57         127           06:45         93         85         134         63         227	04.10		12	138	16	123	28	261		6	83	6	63	12	146
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	04:45		16	158	17	106	33	264		8	94	10	73	18	167
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	05:00		15	167	18	106	33	273		10	104	11	70	21	174
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	05:15		17	153	35	92	52	245		4	83	9	41	13	124
05.35         20         102         96         85         126         137         10         73         32         54         42         127           06:00         42         111         69         88         111         199         16         74         22         58         38         132           06:15         62         107         110         81         1172         188         12         60         32         54         44         144           06:30         85         80         127         68         212         148         19         63         33         64         57         127           06:45         93         85         134         63         227         148         29         64         44         50         73         114           07:00         78         66         114         58         192         124         24         48         32         78         56         126         07:30         90         46         136         46         33         84         48         38         86         70         08:30         88         31         40         38         <	05:30		29	130	48	120	77	250		16	66	18	64	34	130
06:00         42         111         69         88         111         199         16         74         22         58         38         132           06:15         62         107         110         81         172         188         12         60         32         54         44         114           06:45         93         85         134         63         227         148         29         64         44         50         73         114           07:00         78         66         114         58         192         124         24         48         32         78         56         126           07:30         90         46         156         55         246         101         30         46         32         40         62         86           07:45         108         38         143         42         251         80         38         34         48         36         66         70         98:00         38         31         40         38         64         76         98:00         75         52         98:30         86         54         106         105         48	05:45		30	102	96	85	126	187		10	73	32	54	42	127
06:35         62         107         100         85         172         188         12         60         32         54         44         114           06:30         85         80         127         68         212         148         19         63         38         64         57         127           06:45         93         85         134         63         227         148         29         64         44         50         73         114           07:00         78         66         115         45         180         111         24         48         32         78         56         126           07:30         90         46         156         55         246         101         30         46         32         40         62         86           07:30         90         48         24         251         80         38         31         40         38         78         69           08:00         103         42         87         42         190         84         83         34         48         36         86         70         25         28         22         47 <td>06:00</td> <td></td> <td>42</td> <td>111</td> <td>69</td> <td>88</td> <td>111</td> <td>199</td> <td></td> <td>16</td> <td>74</td> <td>22</td> <td>58</td> <td>38</td> <td>132</td>	06:00		42	111	69	88	111	199		16	74	22	58	38	132
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	06:15		62	107	110	81	172	188		12	60	32	54	44	114
06:35         03         85         134         63         227         148         29         64         44         50         73         114           07:00         78         66         114         58         192         124         24         48         32         78         56         126           07:15         66         66         1156         55         246         101         30         46         32         40         62         86           07:30         90         46         156         55         246         101         30         46         32         40         62         86           07:45         108         38         144         42         251         80         38         34         48         36         86         70           08:00         103         42         87         42         190         84         28         38         34         48         36         86         70         05         52         08         38         54         101         59         32         96         66         38         34         53         36         121         70	06:30		85	80	127	68	212	148		19	63	38	64	57	127
07:00         78         66         114         58         192         124         24         48         32         78         56         126           07:15         65         66         115         45         180         111         24         46         29         46         53         92           07:30         90         46         156         55         246         101         30         46         32         40         62         86           07:35         90         46         156         55         246         101         30         46         32         40         38         78         69           08:00         103         42         87         42         190         84         26         38         34         48         86         67         62         86         38         34         48         36         64         76         52         62         33         36         42         110         59         52         62         33         36         121         70         55         52         62         33         132         58         69         39         38	06:45		93	85	134	63	227	148		29	64	44	50	73	114
07:15       65       66       115       43       182       111       24       46       29       46       53       92         07:30       90       46       156       55       246       101       30       46       32       40       62       86         07:45       108       38       143       42       251       80       38       31       40       38       78       69         08:00       103       42       87       42       190       84       26       38       38       64       76         08:15       96       38       110       48       206       86       38       34       48       36       86       70         08:30       88       54       108       51       196       105       28       22       47       30       75       52         08:45       80       35       94       48       174       83       46       33       64       26       110       59         09:00       78       58       88       47       166       105       48       24       48       22       96       46	07:00		78	66	114	58	192	124		24	48	32	78	56	126
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	07:15		65	66	115	45	180	111		24	46	29	46	53	92
07.35       103       38       143       32       251       80       33       31       40       38       78       69         08:00       103       42       87       42       190       84       26       38       31       40       38       78       69         08:00       103       42       87       42       190       84       26       38       31       40       38       78       69         08:15       96       38       110       48       206       86       38       34       48       36       86       70         08:30       88       54       108       196       105       28       22       47       30       75       52         08:45       80       35       94       48       174       83       46       33       64       26       110       59         09:00       78       58       88       47       166       105       48       24       48       22       96       46         09:15       76       51       87       31       166       182       78       82       35       62 </td <td>07:30</td> <td></td> <td>an</td> <td>46</td> <td>156</td> <td>55</td> <td>246</td> <td>101</td> <td></td> <td>30</td> <td>46</td> <td>32</td> <td>40</td> <td>62</td> <td>86</td>	07:30		an	46	156	55	246	101		30	46	32	40	62	86
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	07:45		108	38	143	42	251	80		38	31	40	38	78	69
08:35       96       32       07       42       100       44       100       33       36       36       36       36       36       37       100	08.00		103	42	87	42	190	84		26	38	38	38	64	76
08:30       88       54       108       51       196       105       28       22       47       30       63       105       105         08:45       80       35       94       48       174       83       46       33       64       26       110       59         09:00       78       58       88       47       166       105       48       24       48       22       96       46         09:15       76       51       87       50       163       101       68       34       53       36       121       70         09:30       86       36       80       42       166       78       70       25       62       33       132       58         09:45       121       43       80       38       201       81       80       22       66       22       144       48         10:00       86       39       96       39       182       78       82       35       62       23       144       66         10:30       100       28       78       27       178       55       75       23       73       2	08.00		96	38	110	48	206	86		38	34	48	36	86	70
08:35       80       35       94       48       174       83       46       33       64       26       110       59         09:00       78       58       88       47       166       105       48       24       48       22       96       46         09:00       78       58       88       47       166       105       48       24       48       22       96       46         09:15       76       51       87       50       163       101       68       34       53       36       121       70         09:30       86       36       80       42       166       78       70       25       62       33       132       58         09:45       121       43       80       38       201       81       80       22       66       22       144       48         10:00       86       39       96       39       182       78       82       35       62       23       144       58         10:15       90       27       82       22       172       49       84       87       22       86       21 <td>08.30</td> <td></td> <td>88</td> <td>54</td> <td>108</td> <td>51</td> <td>196</td> <td>105</td> <td></td> <td>28</td> <td>22</td> <td>40</td> <td>30</td> <td>75</td> <td>52</td>	08.30		88	54	108	51	196	105		28	22	40	30	75	52
00:43         00         33         34         43         14         35         46         35         64         20         110         35           09:00         78         58         88         47         166         105         48         24         48         22         96         46           09:15         76         51         87         50         163         101         68         34         53         36         121         70           09:30         86         36         80         42         166         78         70         25         62         33         132         58           09:45         121         43         80         38         201         81         80         22         66         22         144         44           10:0         86         39         96         39         182         78         87         55         75         23         73         28         144         66           10:30         100         28         78         27         178         55         75         23         73         28         148         51	08:45		80	35	94	48	174	83		46	33	64	26	110	50
09:15       76       51       87       50       163       101       68       34       53       36       121       70         09:30       86       36       80       42       166       78       70       25       62       33       132       58         09:45       121       43       80       38       201       81       80       22       66       22       146       44         10:00       86       39       96       39       182       78       82       35       62       23       144       58         10:15       95       32       90       26       185       58       74       38       70       28       144       66         10:30       100       28       78       27       178       55       75       23       73       28       148       51         10:45       90       27       82       22       172       49       84       28       81       26       165       54         11:10       93       26       76       18       169       49       87       22       86       21       173<	09.00		78	58	88	40	166	105		48	24	48	22	96	46
00:10       10       10       10       10       10       10       10       10       11       10       12       11       10       12       14       166       78       71       135       162       163       164       44       165       144       166       144       166       144       165       144       166       144       165       144       165       144       165       144       165       144       165       144       165       144       165       144       165       144       165       144       165       144       165       144       165       144       165       165       164       165       164       165       164       165       164       165       164       165       164 <t< td=""><td>09.15</td><td></td><td>76</td><td>51</td><td>87</td><td>50</td><td>163</td><td>101</td><td></td><td>68</td><td>34</td><td>53</td><td>36</td><td>121</td><td>70</td></t<>	09.15		76	51	87	50	163	101		68	34	53	36	121	70
00:45       121       43       80       38       201       81       80       22       66       22       146       44         10:00       86       39       96       39       182       78       82       35       62       23       144       58         10:15       95       32       90       26       185       58       74       38       70       28       144       58         10:30       100       28       78       27       178       55       75       23       73       28       144       66         10:30       100       28       76       18       169       44       82       8       81       26       165       54         11:00       93       26       76       18       169       44       82       8       80       24       162       32         11:15       102       29       87       20       189       49       87       22       86       21       173       43         11:30       80       22       98       14       226       36       85       16       68       20       153 </td <td>09:30</td> <td></td> <td>86</td> <td>36</td> <td>80</td> <td>42</td> <td>166</td> <td>78</td> <td></td> <td>70</td> <td>25</td> <td>62</td> <td>33</td> <td>132</td> <td>58</td>	09:30		86	36	80	42	166	78		70	25	62	33	132	58
10:00       10:00 <th< td=""><td>09:45</td><td></td><td>121</td><td>43</td><td>80</td><td>38</td><td>201</td><td>81</td><td></td><td>80</td><td>22</td><td>66</td><td>22</td><td>146</td><td>44</td></th<>	09:45		121	43	80	38	201	81		80	22	66	22	146	44
10:15       95       32       90       26       185       58       74       38       70       28       144       66         10:30       100       28       78       27       178       55       75       23       73       28       144       66         10:45       90       27       82       22       172       49       84       28       81       26       165       54         11:00       93       26       76       18       169       44       82       8       80       24       162       32         11:15       102       29       87       20       189       49       87       22       86       21       173       43         11:30       80       22       80       22       160       44       92       19       74       23       166       42         11:45       128       22       98       14       226       36       85       16       68       20       153       36         Total       2419       4222       2743       3546       5162       7768       14420       4204       8624       8624<	10.00		86	39	96	39	182	78		82	35	62	23	144	58
10:30       100       28       78       27       178       55       75       23       73       28       148       51         10:45       90       27       82       22       172       49       84       28       81       26       165       54         11:00       93       26       76       18       169       44       82       8       80       24       162       32         11:15       102       29       87       20       189       49       87       22       86       21       173       43         11:30       80       22       80       22       160       44       92       19       74       23       166       42         11:45       128       22       98       14       226       36       85       16       68       20       153       36         Total       2419       4222       2743       3546       5162       7768       1474       2946       1523       2681       2997       5627         Day Total       18.7%       32.7%       21.2%       27.4%       171%       34.2%       171.7%       31.1%	10:15		95	32	90	26	185	58		74	38	70	28	144	66
10:35       100       27       82       22       172       49       84       28       81       26       165       54         11:00       93       26       76       18       169       44       82       8       80       24       162       32         11:15       102       29       87       20       189       49       87       22       86       21       173       43         11:30       80       22       80       22       160       44       92       19       74       23       166       42         11:45       128       22       98       14       226       36       85       16       68       20       153       36         Total       2419       4222       2743       3546       5162       7768       1474       2946       1523       2681       2997       5627         Day Total       6641       6289       12930       12930       14420       4204       8624       8624         % Total       18.7%       32.7%       21.2%       27.4%       17.1%       34.2%       17.7%       31.1%       94204       8624       8624	10:30		100	28	78	27	178	55		75	23	73	28	148	51
11:00       93       26       76       18       169       44       82       8       80       24       162       32         11:15       102       29       87       20       189       49       87       22       86       21       173       43         11:30       80       22       80       22       160       44       92       19       74       23       166       42         11:45       128       22       98       14       226       36       85       16       68       20       153       36         Total       2419       4222       2743       3546       5162       7768       1474       2946       1523       2681       2997       5627         Day Total       6641       6289       12930       12930       1474       2946       1523       2681       2997       5627         Day Total       18.7%       32.7%       21.2%       27.4%       17.1%       34.2%       17.7%       31.1%         Peak       11:00       03:30       07:00       03:30       07:30       03:30       11:00       10:45       00:45       10:45       01:00	10:45		90	27	82	22	172	49		84	28	81	26	165	54
11:15       102       29       87       20       189       49       87       22       86       21       173       43         11:30       80       22       80       22       160       44       92       19       74       23       166       42         11:45       128       22       98       14       226       36       85       16       68       20       153       36         Total       2419       4222       2743       3546       5162       7768       1474       2946       1523       2681       2997       5627         Day Total       6641       6289       12930       12930       4420       4204       8624       8624         % Total       18.7%       32.7%       21.2%       27.4%       17.1%       34.2%       17.7%       31.1%         Peak       11:00       03:30       07:00       03:30       07:30       03:30       11:00       12:00       10:45       00:45       10:45       01:00         Vol.       403       642       528       457       893       1099       346       376       321       344       666       703	11:00		93	26	76	18	169	44		82		80	24	162	32
11.10       100 <th< td=""><td>11:15</td><td></td><td>102</td><td>29</td><td>87</td><td>20</td><td>189</td><td>49</td><td></td><td>87</td><td>22</td><td>86</td><td>21</td><td>173</td><td>43</td></th<>	11:15		102	29	87	20	189	49		87	22	86	21	173	43
11:00         128         22         98         14         226         36         85         16         17         120         153         36           Total         2419         4222         2743         3546         5162         7768         1474         2946         1523         2681         2997         5627           Day Total         6641         6289         12930         14420         4204         8624         8624           % Total         18.7%         32.7%         21.2%         27.4%         17.1%         34.2%         17.7%         31.1%           Peak         11:00         03:30         07:00         03:30         07:30         03:30         11:00         12:00         10:45         00:45         10:45         01:00           Vol.         403         642         528         457         893         1099         346         376         321         344         666         703           P.H.F.         0.787         0.933         0.846         0.810         0.889         0.901         0.940         0.825         0.933         0.962         0.976	11:30		80	22	80	22	160	40		92	19	74	23	166	40
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	P.H.F		0.787	0.933	0.846	0.810	0.889	0.901		0.940	0.825	0.933	0.956	0.962	0.976
			-			_									

ADT ADT 10,768 AADT 10,768

Page 1

## Innovative Data, LLC

Location: Southampton Road Location: South of North Road Location: Westfield, Massachusetts Client: VHB / J. Locke

PO Box 468 Belchertown, Massachusetts innovativedatallc.com or 1.413.668.5094

$\begin{array}{c c c c c c c c c c c c c c c c c c c $		Start	Fri	25-Jan-13	Sat	26-Jan-13	Sun	27-Jan-13	Daily	y Average
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Vol.         836         1068         698         745         749         856           P.H.F.         0.889         0.934         0.948         0.904         0.975         0.930           ADT         ADT 10,441         AADT 10,441         AADT 10,441         0.904         0.975         0.930	-	Peak	07:30	03:30	11.00	01.15			11.00	04.15
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ITE Trip Generation Worksheets LUC 945 "Gasoline/Service Station with Convenience Market" VHB Calculations

## Land Use: 945 Gasoline/Service Station with Convenience Market

## Description

This land use includes gasoline/service stations with convenience markets where the primary business is the fueling of motor vehicles. These service stations may also have ancillary facilities for servicing and repairing motor vehicles. Some commonly sold convenience items are newspapers, coffee or other beverages and snack items that are usually consumed in the car. These service stations are generally located at intersections or interchanges. This land use does not include stations with car washes. Convenience market (open 24 hours) (Land Use 851), convenience market (open 15-16 hours) (Land Use 852), convenience market with gasoline pumps (Land Use 853), gasoline/service station (Land Use 944), gasoline/service station with convenience market and car wash (Land Use 946) and truck stop (Land Use 950) are related uses.

## **Additional Data**

For the purpose of this land use, the independent variable, vehicle fueling positions, is defined as the maximum number of vehicles that can be fueled simultaneously.

Gasoline/service stations in this land use include "pay-at-the-pump" and traditional fueling stations.

The weekday peak hours of the generator typically coincided with the peak hours of the adjacent street traffic.

The sites were surveyed between the late 1980s and the 2000s throughout the United States, with many conducted in New England.

## Source Numbers

221, 255, 288, 347, 350, 351, 355, 440, 631, 718

# Gasoline/Service Station with Convenience Market (945)

Average Vehicle Trip Ends vs: Vehicle Fueling Positions On a: Weekday

Number of Studies: 11 Average Vehicle Fueling Positions: 12 Directional Distribution: 50% entering, 50% exiting

## **Trip Generation per Vehicle Fueling Position**

Average Rate	Range of Rates	Standard Deviation
162.78	90.67 - 299.50	68.16

## Data Plot and Equation



# Gasoline/Service Station with Convenience Market (945)

Average Vehicle Trip Ends vs: On a:	Vehicle Fueling Positions Weekday, Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m.
Number of Studies:	39
Average Vehicle Fueling Positions:	10
Directional Distribution:	50% entering, 50% exiting

## **Trip Generation per Vehicle Fueling Position**

Average Rate	Range of Rates	Standard Deviation
13.51	4.25 - 57.80	7.91

## **Data Plot and Equation**



## Land Use: 820 Shopping Center

## Description

A shopping center is an integrated group of commercial establishments that is planned, developed, owned and managed as a unit. A shopping center's composition is related to its market area in terms of size, location and type of store. A shopping center also provides on-site parking facilities sufficient to serve its own parking demands. Specialty retail center (Land Use 826) and factory outlet center (Land Use 823) are related uses.

## **Additional Data**

Shopping centers, including neighborhood centers, community centers, regional centers and super regional centers, were surveyed for this land use. Some of these centers contained nonmerchandising facilities, such as office buildings, movie theaters, restaurants, post offices, banks, health clubs and recreational facilities (for example, ice skating rinks or indoor miniature golf courses). The centers ranged in size from 1,700 to 2.2 million square feet gross leasable area (GLA). The centers studied were located in suburban areas throughout the United States and, therefore, represent typical U.S. suburban conditions.

Many shopping centers, in addition to the integrated unit of shops in one building or enclosed around a mall, include outparcels (peripheral buildings or pads located on the perimeter of the center adjacent to the streets and major access points). These buildings are typically drivein banks, retail stores, restaurants, or small offices. Although the data herein do not indicate which of the centers studied included peripheral buildings, it can be assumed that some of the data show their effect.

The vehicle trips generated at a shopping center are based upon the total GLA of the center. In cases of smaller centers without an enclosed mall or peripheral buildings, the GLA could be the same as the gross floor area of the building.

Separate equations have been developed for shopping centers during the Christmas shopping season. Plots were included for the weekday peak hour of adjacent street traffic and the Saturday peak hour of the generator.

Information on approximate hourly, monthly and daily variation in shopping center traffic is shown in Tables 1–3. It should be noted, however, that the information contained in these tables is based on a limited sample size. Therefore, caution should be exercised when applying the data. Also, some information provided in the tables may conflict with the results obtained by applying the average rate or regression equations. When this occurs, it is suggested that the results from the average rate or regression equations be used, as they are based on a larger number of studies.

# Shopping Center (820)

### Average Vehicle Trip Ends vs: 1000 Sq. Feet Gross Leasable Area On a: Weekday

Number of Studies: 302 Average 1000 Sq. Feet GLA: 331 Directional Distribution: 50% entering, 50% exiting

## Trip Generation per 1000 Sq. Feet Gross Leasable Area

Average Rate	Range of Rates	Standard Deviation
42.70	12.50 - 270.89	21.25

## **Data Plot and Equation**



# Shopping Center<br/>(820)Average Vehicle Trip Ends vs:1000 Sq. Feet Gross Leasable Area<br/>On a:Weekday,<br/>Peak Hour of Adjacent Street Traffic,<br/>One Hour Between 4 and 6 p.m.Number of Studies:426<br/>Average 1000 Sq. Feet GLA:Average 1000 Sq. Feet GLA:376<br/>Directional Distribution:48% entering, 52% exiting

## Trip Generation per 1000 Sq. Feet Gross Leasable Area

Average Rate	Range of Rates	Standard Deviation
3.71	0.68 - 29.27	2.74

## **Data Plot and Equation**



Trip Generation, 9th Edition 
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## Shopping Center (820)

## Average Vehicle Trip Ends vs: 1000 Sq. Feet Gross Leasable Area On a: Saturday

Number of Studies: 123 Average 1000 Sq. Feet GLA: 450 Directional Distribution: 50% entering, 50% exiting

## Trip Generation per 1000 Sq. Feet Gross Leasable Area

Average Rate	Range of Rates	Standard Deviation
49.97	16.70 - 227.50	22.62

## **Data Plot and Equation**



# Shopping Center (820)

## Average Vehicle Trip Ends vs: 1000 Sq. Feet Gross Leasable Area On a: Saturday, Peak Hour of Generator

Number of Studies: 128 Average 1000 Sq. Feet GLA: 458 Directional Distribution: 52% entering, 48% exiting

## Trip Generation per 1000 Sq. Feet Gross Leasable Area

Average Rate	Range of Rates	Standard Deviation
4.82	1.46 - 18.32	3.10

## **Data Plot and Equation**



Trip Generation, 9th Edition • Institute of Transportation Engineers 1565 **Computations** 

Project: VF	Project # 41827,00
Location: Westfield	Sheet ( of 2
Calculated by: JLL	Date: 2/4/2013
Checked by:	Date:
Title Trip Generation	laculations



VHB Computations

Project:	Project #
Location:	Sheet 2 of 2
Calculated by:	Date:
Checked by:	Date:
Title	

Saturday	Pairy: ava	age rate / Ks	= = 49.97
	36.4 KJF;	× 49.97 =	1820 trips
Saturday P.	care Hour: (	average rate /	KSF = 4.82
	36.9 KSF	x 4.62 =	175 this
		(90	enter/osexit)
Summary To	ble :		
	Luc 945	Pass-by	Total New
weekday	1630	410	1220
ucekday PM			
enter	70	20	50
exit	65	15 35	50
Saturday	1820	460	1360
Satuday.	90	25	65
midday	85	20	65
	175	45	130

## Crash Data

2008-2010 Crash Summary Crash Rate Worksheet

## Vehicular Crash Summary (2008 - 2010)

	(1000 1010)				
	Southampton Road at North Road	Total			
Year					
2008	6	6			
2009	5	5			
2010	11	11			
Total	22	22			
Average	7.33	7.33			
Collision Type					
Angle	9	9			
Head-on	1	1			
Rear-end	7	7			
Rear-to-Rear	0	0			
Sideswine, opposite direction	0	0			
Sideswipe, opposite direction	0	2			
Single vehicle crach	2	2			
	2	2			
Not reported	U 1	1			
	1	1			
lotai	22	22			
Crash Severity					
Fatal injury	0	0			
Non-fatal injury	10	10			
Property damage only (none injured)	12	12			
Not Reported	0	0			
Unknown	0	0			
Total	22	22			
7					
Time of Day					
Weekday, 7:00 AM - 9:00 AM	2	2			
Weekday, 4:00 PM - 6:00 PM	6	6			
Saturday, 11:00 AM - 2:00 PM	0	0			
Weekday, other time	9	9			
Weekend, other time	5	5			
Total	22	22			
Pavement Conditions					
Dry	19	19			
Wet	3	3			
Snow	0	0			
Ice	0	0			
Sand, mud, dirt, oil, gravel	0	0			
Water (standing, moving)	0	0			
Slush	0	0			
Other	0	0			
Unknown	0	0			
Not reported	0	0			
Total	22	22			
Non Motroist (Bike, Pedestrian)		0			
ו טנמו	U	U			
MassHighway Crash Rates	1.14	1.14			



## INTERSECTION CRASH RATE WORKSHEET

CITY/TOWN : WES	TFIELD	, MA		COUNT DA	TE: 1/2	4/2013
DISTRICT : 2	UNSIGN	IALIZED :		SIGNA	ALIZED :	YES
,		~ IN	TERSECTIO	N DATA ~		
MAJOR STREET :	SOL	ITHAMP	TON	ROAD	(Route	= 10/202
MINOR STREET(S) :	NO	RTH	ZOAD	(POUTE	202	)
				5	И	
INTERSECTION	↑ North			SOUT	HAMPTO	N
DIAGRAM (Label Approaches)					1	(2) NORTH
	No	RTH -				202
			3	) Sout	0/202 THAMPT	Lnc
			PEAK HOUI	R VOLUMES		Total Peak
APPROACH :	1	2	3	4	5	Hourly
DIRECTION :	SB	WB	NB	EB		Approacn Volume
VOLUMES (AMPM):	282	497	638	116		1533
"K" FACTOR:	,087	INTERS	ECTION ADT APPROACH	( <b>V</b> )= TOTA I VOLUME:	AL DAILY	17620
TOTAL # OF CRASHES :	22	# OF YEARS :	3	AVERA CRASHES A	GE # OF PER YEAR ( ) :	7.33
CRASH RATE CALCU	LATION :	1.14	RATE =	<u>(A*1,0</u> (V)	000,000 ) ' 365 )	
Comments : Project Title & Date:	CF -	10 fuel	ng posti	tions		

# Operational Analyses Intersection Capacity Analysis

## Queues 16: North Road & Southampton Road

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Lane Group	EBL	EBT	WBL	WBT	WBR	NBL	NBT	SBL	SBT	
Lane Configurations		4		ជ	1		4		4	
Volume (vph)	15	70	195	160	155	30	300	60	210	
Lane Group Flow (vph)	0	125	0	395	172	0	768	0	324	
Turn Type	Perm		Perm		Perm	Perm		Perm		
Protected Phases		4		8			2		6	
Permitted Phases	4		8		8	2		6		
Detector Phase	4	4	8	8	8	2	2	6	6	
Switch Phase										
Minimum Initial (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	
Minimum Split (s)	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0	
Total Split (s)	30.0	30.0	30.0	30.0	30.0	35.0	35.0	35.0	35.0	
Total Split (%)	46.2%	46.2%	46.2%	46.2%	46.2%	53.8%	53.8%	53.8%	53.8%	
Yellow Time (s)	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	
All-Red Time (s)	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	
Lead/Lag										
Lead-Lag Optimize?										
Recall Mode	None	None	None	None	None	Min	Min	Min	Min	
v/c Ratio		0.20		0.76	0.26		0.88		0.45	
Control Delay		10.9		26.7	3.6		26.0		12.6	
Queue Delay		0.0		0.0	0.0		0.0		0.0	
Total Delay		10.9		26.7	3.6		26.0		12.6	
Queue Length 50th (ft)		22		125	0		198		68	
Queue Length 95th (ft)		53		219	32		#401		136	
Internal Link Dist (ft)		455		249			573		237	
Turn Bay Length (ft)										
Base Capacity (vph)		830		716	856		1044		876	
Starvation Cap Reductn		0		0	0		0		0	
Spillback Cap Reductn		0		0	0		0		0	
Storage Cap Reductn		0		0	0		0		0	
Reduced v/c Ratio		0.15		0.55	0.20		0.74		0.37	
Intersection Summary										
Cycle Length: 65										
Actuated Cycle Length: 55.4	1									
Natural Cycle: 50										
Control Type: Actuated-Unc	oordinated	d								
# 95th percentile volume e	exceeds ca	apacity, q	ueue may	be longe	er.					
Queue shown is maximu	m after tw	o cycles.								
		0 0 <i>1</i> /								
Splits and Phases: 16: No	orth Road	& Southa	mpton Ro	ad						

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35 s	30 s

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		\$			र्स	1		\$			\$	
Volume (vph)	15	70	30	195	160	155	30	300	315	60	210	15
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		4.0			4.0	4.0		4.0			4.0	
Lane Util. Factor		1.00			1.00	1.00		1.00			1.00	
Frt		0.96			1.00	0.85		0.93			0.99	
Flt Protected		0.99			0.97	1.00		1.00			0.99	
Satd. Flow (prot)		1734			1778	1553		1736			1830	
Flt Permitted		0.94			0.79	1.00		0.98			0.80	
Satd. Flow (perm)		1640			1446	1553		1697			1478	
Peak-hour factor, PHF	0.92	0.92	0.92	0.90	0.90	0.90	0.84	0.84	0.84	0.88	0.88	0.88
Adj. Flow (vph)	16	76	33	217	178	172	36	357	375	68	239	17
RTOR Reduction (vph)	0	21	0	0	0	109	0	52	0	0	3	0
Lane Group Flow (vph)	0	104	0	0	395	63	0	716	0	0	321	0
Heavy Vehicles (%)	5%	5%	5%	4%	4%	4%	2%	2%	2%	2%	2%	2%
Turn Type	Perm			Perm		Perm	Perm			Perm		
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		
Actuated Green, G (s)		20.0			20.0	20.0		26.9			26.9	
Effective Green, g (s)		20.0			20.0	20.0		26.9			26.9	
Actuated g/C Ratio		0.36			0.36	0.36		0.49			0.49	
Clearance Time (s)		4.0			4.0	4.0		4.0			4.0	
Vehicle Extension (s)		3.0			3.0	3.0		3.0			3.0	
Lane Grp Cap (vph)		597			527	566		831			724	
v/s Ratio Prot												
v/s Ratio Perm		0.06			c0.27	0.04		c0.42			0.22	
v/c Ratio		0.17			0.75	0.11		0.86			0.44	
Uniform Delay, d1		11.8			15.3	11.6		12.4			9.1	
Progression Factor		1.00			1.00	1.00		1.00			1.00	
Incremental Delay, d2		0.1			5.8	0.1		9.2			0.4	
Delay (s)		12.0			21.1	11.6		21.5			9.6	
Level of Service		В			С	В		С			А	
Approach Delay (s)		12.0			18.2			21.5			9.6	
Approach LOS		В			В			С			А	
Intersection Summary												
HCM Average Control Delay			17.6	Н	CM Level	l of Servic	e		В			
HCM Volume to Capacity ratio			0.81									
Actuated Cycle Length (s)			54.9	S	um of los	t time (s)			8.0			
Intersection Capacity Utilization	1		71.3%	IC	CU Level	of Service	,		С			
Analysis Period (min)			15									

c Critical Lane Group

## Queues 16: North Road & Southampton Road

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Lane Group	EBL	EBT	WBL	WBT	WBR	NBL	NBT	SBL	SBT	
Lane Configurations		4		ર્સ	1		4		4	
Volume (vph)	10	105	140	50	65	30	185	105	175	
Lane Group Flow (vph)	0	159	0	232	79	0	473	0	298	
Turn Type	Perm		Perm		Perm	Perm		Perm		
Protected Phases		4		8			2		6	
Permitted Phases	4		8		8	2		6		
Detector Phase	4	4	8	8	8	2	2	6	6	
Switch Phase										
Minimum Initial (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	
Minimum Split (s)	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0	
Total Split (s)	30.0	30.0	30.0	30.0	30.0	35.0	35.0	35.0	35.0	
Total Split (%)	46.2%	46.2%	46.2%	46.2%	46.2%	53.8%	53.8%	53.8%	53.8%	
Yellow Time (s)	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	
All-Red Time (s)	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	
Lead/Lag										
Lead-Lag Optimize?										
Recall Mode	None	None	None	None	None	Min	Min	Min	Min	
v/c Ratio		0.26		0.51	0.14		0.59		0.47	
Control Delay		9.4		14.8	3.9		10.2		11.1	
Queue Delay		0.0		0.0	0.0		0.0		0.0	
Total Delay		9.4		14.8	3.9		10.2		11.1	
Queue Length 50th (ft)		15		29	0		42		34	
Queue Length 95th (ft)		61		92	17		152		115	
Internal Link Dist (ft)		455		249			573		237	
Turn Bay Length (ft)										
Base Capacity (vph)		1308		1012	1167		1445		1225	
Starvation Cap Reductn		0		0	0		0		0	
Spillback Cap Reductn		0		0	0		0		0	
Storage Cap Reductn		0		0	0		0		0	
Reduced v/c Ratio		0.12		0.23	0.07		0.33		0.24	
Intersection Summary										
Cycle Length: 65										
Actuated Cycle Length: 37.4										
Natural Cycle: 40										
Control Type: Actuated-Unco	ordinated									
//**										

Splits and Phases: 16: North Road & Southampton Road

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35 s	30 s

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		\$			र्स	1		\$			\$	
Volume (vph)	10	105	30	140	50	65	30	185	225	105	175	10
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		4.0			4.0	4.0		4.0			4.0	
Lane Util. Factor		1.00			1.00	1.00		1.00			1.00	
Frt		0.97			1.00	0.85		0.93			1.00	
Flt Protected		1.00			0.96	1.00		1.00			0.98	
Satd. Flow (prot)		1804			1762	1553		1728			1821	
Flt Permitted		0.97			0.75	1.00		0.97			0.78	
Satd. Flow (perm)		1764			1372	1553		1677			1439	
Peak-hour factor, PHF	0.91	0.91	0.91	0.82	0.82	0.82	0.93	0.93	0.93	0.97	0.97	0.97
Adj. Flow (vph)	11	115	33	171	61	79	32	199	242	108	180	10
RTOR Reduction (vph)	0	16	0	0	0	52	0	61	0	0	2	0
Lane Group Flow (vph)	0	143	0	0	232	27	0	412	0	0	296	0
Heavy Vehicles (%)	2%	2%	2%	4%	4%	4%	2%	2%	2%	2%	2%	2%
Turn Type	Perm			Perm		Perm	Perm			Perm		
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		
Actuated Green, G (s)		12.4			12.4	12.4		16.5			16.5	
Effective Green, g (s)		12.4			12.4	12.4		16.5			16.5	
Actuated g/C Ratio		0.34			0.34	0.34		0.45			0.45	
Clearance Time (s)		4.0			4.0	4.0		4.0			4.0	
Vehicle Extension (s)		3.0			3.0	3.0		3.0			3.0	
Lane Grp Cap (vph)		593			461	522		750			643	
v/s Ratio Prot												
v/s Ratio Perm		0.08			c0.17	0.02		c0.25			0.21	
v/c Ratio		0.24			0.50	0.05		0.55			0.46	
Uniform Delay, d1		8.9			9.8	8.3		7.5			7.1	
Progression Factor		1.00			1.00	1.00		1.00			1.00	
Incremental Delay, d2		0.2			0.9	0.0		0.8			0.5	
Delay (s)		9.1			10.7	8.3		8.3			7.6	
Level of Service		А			В	А		А			А	
Approach Delay (s)		9.1			10.1			8.3			7.6	
Approach LOS		А			В			A			А	
Intersection Summary												
HCM Average Control Delay			8.7	Н	CM Level	of Servic	e		А			
HCM Volume to Capacity ratio			0.53									
Actuated Cycle Length (s)			36.9	S	um of los	t time (s)			8.0			
Intersection Capacity Utilization	ı		72.4%	IC	CU Level	of Service			С			
Analysis Period (min)			15									

c Critical Lane Group

## Queues 16: North Road & Southampton Road

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Lane Group	EBL	EBT	WBL	WBT	WBR	NBL	NBT	SBL	SBT	
Lane Configurations		4		្រា	1		4		4	
Volume (vph)	15	75	215	175	170	35	330	65	230	
Lane Group Flow (vph)	0	136	0	433	189	0	852	0	352	
Turn Type	Perm		Perm		Perm	Perm		Perm		
Protected Phases		4	-	8	-	-	2	-	6	
Permitted Phases	4		8		8	2		6		
Detector Phase	4	4	8	8	8	2	2	6	6	
Switch Phase										
Minimum Initial (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	
Minimum Split (s)	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0	
Total Split (s)	30.0	30.0	30.0	30.0	30.0	35.0	35.0	35.0	35.0	
Total Split (%)	46.2%	46.2%	46.2%	46.2%	46.2%	53.8%	53.8%	53.8%	53.8%	
Yellow Time (s)	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	
All-Red Time (s)	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	
Lead/Lag										
Lead-Lag Optimize?										
Recall Mode	None	None	None	None	None	Min	Min	Min	Min	
v/c Ratio		0.23		0.87	0.28		0.93		0.48	
Control Delay		11.0		37.3	3.6		32.6		13.3	
Queue Delay		0.0		0.0	0.0		0.0		0.0	
Total Delay		11.0		37.3	3.6		32.6		13.3	
Queue Length 50th (ft)		25		143	0		262		82	
Queue Length 95th (ft)		57		#283	33		#478		154	
Internal Link Dist (ft)		455		249			573		237	
Turn Bay Length (ft)										
Base Capacity (vph)		728		617	779		921		735	
Starvation Cap Reductn		0		0	0		0		0	
Spillback Cap Reductn		0		0	0		0		0	
Storage Cap Reductn		0		0	0		0		0	
Reduced v/c Ratio		0.19		0.70	0.24		0.93		0.48	
Intersection Summary										
Cycle Length: 65										
Actuated Cycle Length: 60.5										
Natural Cycle: 55										
Control Type: Actuated-Unco	ordinated									
# 95th percentile volume ex	ceeds ca	pacity, qu	ueue may	be longe	er.					
Queue shown is maximum	n after two	o cycles.								
Splits and Phases: 16: Nor	th Road <sup>y</sup>	& Southa	moton Ro	ad						

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			ર્સ	1		4			\$	
Volume (vph)	15	75	35	215	175	170	35	330	350	65	230	15
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		4.0			4.0	4.0		4.0			4.0	
Lane Util. Factor		1.00			1.00	1.00		1.00			1.00	
Frt		0.96			1.00	0.85		0.93			0.99	
Flt Protected		0.99			0.97	1.00		1.00			0.99	
Satd. Flow (prot)		1731			1778	1553		1735			1831	
Flt Permitted		0.94			0.78	1.00		0.97			0.77	
Satd. Flow (perm)		1637			1424	1553		1689			1422	
Peak-hour factor, PHF	0.92	0.92	0.92	0.90	0.90	0.90	0.84	0.84	0.84	0.88	0.88	0.88
Adj. Flow (vph)	16	82	38	239	194	189	42	393	417	74	261	17
RTOR Reduction (vph)	0	23	0	0	0	123	0	49	0	0	2	0
Lane Group Flow (vph)	0	113	0	0	433	66	0	803	0	0	350	0
Heavy Vehicles (%)	5%	5%	5%	4%	4%	4%	2%	2%	2%	2%	2%	2%
Turn Type	Perm			Perm		Perm	Perm			Perm		
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		
Actuated Green, G (s)		21.2			21.2	21.2		31.2			31.2	
Effective Green, g (s)		21.2			21.2	21.2		31.2			31.2	
Actuated g/C Ratio		0.35			0.35	0.35		0.52			0.52	
Clearance Time (s)		4.0			4.0	4.0		4.0			4.0	
Vehicle Extension (s)		3.0			3.0	3.0		3.0			3.0	
Lane Grp Cap (vph)		575			500	545		872			735	
v/s Ratio Prot												
v/s Ratio Perm		0.07			c0.30	0.04		c0.48			0.25	
v/c Ratio		0.20			0.87	0.12		0.92			0.48	
Uniform Delay, d1		13.7			18.3	13.3		13.5			9.4	
Progression Factor		1.00			1.00	1.00		1.00			1.00	
Incremental Delay, d2		0.2			14.5	0.1		14.8			0.5	
Delay (s)		13.8			32.8	13.4		28.2			9.8	
Level of Service		В			С	В		С			А	
Approach Delay (s)		13.8			26.9			28.2			9.8	
Approach LOS		В			С			С			А	
Intersection Summary												
HCM Average Control Delay			23.5	Н	CM Leve	l of Servic	e		С			
HCM Volume to Capacity ratio			0.90									
Actuated Cycle Length (s)			60.4	S	um of los	t time (s)			8.0			
Intersection Capacity Utilization	า		77.5%	IC	U Level	of Service			D			
Analysis Period (min)			15									

c Critical Lane Group

## Queues 16: North Road & Southampton Road

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Lane Group	EBL	EBT	WBL	WBT	WBR	NBL	NBT	SBL	SBT	
Lane Configurations		\$		र्स	1		\$		\$	
Volume (vph)	10	115	155	55	70	35	205	115	195	
Lane Group Flow (vph)	0	175	0	256	85	0	527	0	330	
Turn Type	Perm		Perm		Perm	Perm		Perm		
Protected Phases		4		8			2		6	
Permitted Phases	4		8		8	2		6		
Detector Phase	4	4	8	8	8	2	2	6	6	
Switch Phase										
Minimum Initial (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	
Minimum Split (s)	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0	
Total Split (s)	30.0	30.0	30.0	30.0	30.0	35.0	35.0	35.0	35.0	
Total Split (%)	46.2%	46.2%	46.2%	46.2%	46.2%	53.8%	53.8%	53.8%	53.8%	
Yellow Time (s)	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	
All-Red Time (s)	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	
Lead/Lag										
Lead-Lag Optimize?										
Recall Mode	None	None	None	None	None	Min	Min	Min	Min	
v/c Ratio		0.29		0.57	0.15		0.65		0.53	
Control Delay		10.6		17.4	4.1		11.9		12.6	
Queue Delay		0.0		0.0	0.0		0.0		0.0	
Total Delay		10.6		17.4	4.1		11.9		12.6	
Queue Length 50th (ft)		19		37	0		55		42	
Queue Length 95th (ft)		76		117	19		199		146	
Internal Link Dist (ft)		455		249			573		237	
Turn Bay Length (ft)										
Base Capacity (vph)		1252		952	1120		1378		1124	
Starvation Cap Reductn		0		0	0		0		0	
Spillback Cap Reductn		0		0	0		0		0	
Storage Cap Reductn		0		0	0		0		0	
Reduced v/c Ratio		0.14		0.27	0.08		0.38		0.29	
Intersection Summary										
Cycle Length: 65										
Actuated Cycle Length: 40.3										
Natural Cycle: 40										
Control Type: Actuated-Unco	ordinated	I								

Splits and Phases: 16: North Road & Southampton Road

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		\$			ę	1		\$			\$	
Volume (vph)	10	115	35	155	55	70	35	205	250	115	195	10
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		4.0			4.0	4.0		4.0			4.0	
Lane Util. Factor		1.00			1.00	1.00		1.00			1.00	
Frt		0.97			1.00	0.85		0.93			1.00	
Flt Protected		1.00			0.96	1.00		1.00			0.98	
Satd. Flow (prot)		1802			1762	1553		1728			1822	
Flt Permitted		0.98			0.74	1.00		0.96			0.74	
Satd. Flow (perm)		1765			1350	1553		1667			1379	
Peak-hour factor, PHF	0.91	0.91	0.91	0.82	0.82	0.82	0.93	0.93	0.93	0.97	0.97	0.97
Adj. Flow (vph)	11	126	38	189	67	85	38	220	269	119	201	10
RTOR Reduction (vph)	0	17	0	0	0	56	0	60	0	0	2	0
Lane Group Flow (vph)	0	158	0	0	256	29	0	467	0	0	328	0
Heavy Vehicles (%)	2%	2%	2%	4%	4%	4%	2%	2%	2%	2%	2%	2%
Turn Type	Perm			Perm		Perm	Perm			Perm		
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		
Actuated Green, G (s)		13.5			13.5	13.5		18.1			18.1	
Effective Green, g (s)		13.5			13.5	13.5		18.1			18.1	
Actuated g/C Ratio		0.34			0.34	0.34		0.46			0.46	
Clearance Time (s)		4.0			4.0	4.0		4.0			4.0	
Vehicle Extension (s)		3.0			3.0	3.0		3.0			3.0	
Lane Grp Cap (vph)		602			460	529		762			630	
v/s Ratio Prot												
v/s Ratio Perm		0.09			c0.19	0.02		c0.28			0.24	
v/c Ratio		0.26			0.56	0.05		0.61			0.52	
Uniform Delay, d1		9.4			10.6	8.8		8.1			7.7	
Progression Factor		1.00			1.00	1.00		1.00			1.00	
Incremental Delay, d2		0.2			1.5	0.0		1.5			0.8	
Delay (s)		9.7			12.1	8.8		9.6			8.4	
Level of Service		А			В	А		А			А	
Approach Delay (s)		9.7			11.3			9.6			8.4	
Approach LOS		А			В			А			А	
Intersection Summary												
HCM Average Control Delay			9.7	Н	CM Level	l of Servic	e		А			
HCM Volume to Capacity ratio			0.59									
Actuated Cycle Length (s)			39.6	S	um of los	t time (s)			8.0			
Intersection Capacity Utilization	1		78.8%	IC	CU Level of	of Service			D			
Analysis Period (min)			15									

c Critical Lane Group

## Queues 1: North Road & Southampton Road

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Lane Group	EBL	EBT	WBL	WBT	WBR	NBL	NBT	SBL	SBT	
Lane Configurations		4		ដ	1		4		4	
Volume (vph)	20	80	225	180	170	35	335	65	235	
Lane Group Flow (vph)	0	147	0	450	189	0	870	0	364	
Turn Type	Perm		Perm		Perm	Perm		Perm		
Protected Phases		4		8			2		6	
Permitted Phases	4		8		8	2		6		
Detector Phase	4	4	8	8	8	2	2	6	6	
Switch Phase										
Minimum Initial (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	
Minimum Split (s)	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0	
Total Split (s)	30.0	30.0	30.0	30.0	30.0	35.0	35.0	35.0	35.0	
Total Split (%)	46.2%	46.2%	46.2%	46.2%	46.2%	53.8%	53.8%	53.8%	53.8%	
Yellow Time (s)	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	
All-Red Time (s)	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	
Lead/Lag										
Lead-Lag Optimize?										
Recall Mode	None	None	None	None	None	Min	Min	Min	Min	
v/c Ratio		0.24		0.89	0.28		0.96		0.51	
Control Delay		11.5		39.8	3.5		38.8		14.1	
Queue Delay		0.0		0.0	0.0		0.0		0.0	
I otal Delay		11.5		39.8	3.5		38.8		14.1	
Queue Length 50th (ft)		28		152	0		~310		93	
Queue Length 95th (ft)		63		#304	33		#493		161	
Internal Link Dist (ft)		42		249			1		237	
Turn Bay Length (ft)		700		507	700		007		740	
Base Capacity (vph)		700		597	769		907		/16	
Starvation Cap Reductn		0		0	0		0		0	
Spiliback Cap Reductin		0		0	0		0		0	
Storage Cap Reductn		0		0 75	0		0		0	
Reduced V/C Ratio		0.21		0.75	0.25		0.96		0.51	
Intersection Summary										
Cycle Length: 65										
Actuated Cycle Length: 61.5										
Natural Cycle: 60										
Control Type: Actuated-Unco	ordinated									
<ul> <li>Volume exceeds capacity</li> </ul>	, queue i	s theoreti	cally infin	ite.						
Queue shown is maximum	n after two	o cycles.								

# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles. Splits and Phases: 1: North Road & Southampton Road

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35 s	30 s

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		\$			र्स	1		\$			\$	
Volume (vph)	20	80	35	225	180	170	35	335	360	65	235	20
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		4.0			4.0	4.0		4.0			4.0	
Lane Util. Factor		1.00			1.00	1.00		1.00			1.00	
Frt		0.97			1.00	0.85		0.93			0.99	
Flt Protected		0.99			0.97	1.00		1.00			0.99	
Satd. Flow (prot)		1733			1778	1553		1735			1828	
Flt Permitted		0.92			0.77	1.00		0.97			0.76	
Satd. Flow (perm)		1601			1403	1553		1688			1405	
Peak-hour factor, PHF	0.92	0.92	0.92	0.90	0.90	0.90	0.84	0.84	0.84	0.88	0.88	0.88
Adj. Flow (vph)	22	87	38	250	200	189	42	399	429	74	267	23
RTOR Reduction (vph)	0	20	0	0	0	120	0	51	0	0	3	0
Lane Group Flow (vph)	0	127	0	0	450	69	0	819	0	0	361	0
Heavy Vehicles (%)	5%	5%	5%	4%	4%	4%	2%	2%	2%	2%	2%	2%
Turn Type	Perm			Perm		Perm	Perm			Perm		
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		
Actuated Green, G (s)		22.3			22.3	22.3		31.2			31.2	
Effective Green, g (s)		22.3			22.3	22.3		31.2			31.2	
Actuated g/C Ratio		0.36			0.36	0.36		0.51			0.51	
Clearance Time (s)		4.0			4.0	4.0		4.0			4.0	
Vehicle Extension (s)		3.0			3.0	3.0		3.0			3.0	
Lane Grp Cap (vph)		581			509	563		856			713	
v/s Ratio Prot												
v/s Ratio Perm		0.08			c0.32	0.04		c0.49			0.26	
v/c Ratio		0.22			0.88	0.12		0.96			0.51	
Uniform Delay, d1		13.6			18.4	13.1		14.5			10.0	
Progression Factor		1.00			1.00	1.00		1.00			1.00	
Incremental Delay, d2		0.2			16.5	0.1		20.8			0.6	
Delay (s)		13.8			34.9	13.2		35.3			10.6	
Level of Service		В			С	В		D			В	
Approach Delay (s)		13.8			28.5			35.3			10.6	
Approach LOS		В			С			D			В	
Intersection Summary												
HCM Average Control Delay			27.1	Н	CM Level	of Servic	e		С			
HCM Volume to Capacity ratio			0.93									
Actuated Cycle Length (s)			61.5	S	um of lost	t time (s)			8.0			
Intersection Capacity Utilization	1		79.4%	IC	CU Level o	of Service			D			
Analysis Period (min)			15									

c Critical Lane Group

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Movement	EBL	EBR	NBL	NBT	SBT	SBR	
Lane Configurations	Y			र्स	eî.		
Volume (veh/h)	20	25	20	715	475	5	
Sign Control	Stop			Free	Free		
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	22	27	22	777	516	5	
Pedestrians							
Lane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)							
Median type				None	None		
Median storage veh)							
Upstream signal (ft)					258		
pX, platoon unblocked	0.93	0.93	0.93				
vC, conflicting volume	1340	519	522				
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	1328	450	452				
tC, single (s)	6.4	6.2	4.1				
tC, 2 stage (s)							
tF (s)	3.5	3.3	2.2				
p0 queue free %	86	95	98				
cM capacity (veh/h)	156	569	1035				
Direction, Lane #	EB 1	NB 1	SB 1				
Volume Total	49	799	522				
Volume Left	22	22	0				
Volume Right	27	0	5				
cSH	262	1035	1700				
Volume to Capacity	0.19	0.02	0.31				
Queue Length 95th (ft)	17	2	0				
Control Delay (s)	21.9	0.6	0.0				
Lane LOS	С	А					
Approach Delay (s)	21.9	0.6	0.0				
Approach LOS	С						
Intersection Summary							
Average Delay			1.1				
Intersection Capacity Utilization	on		63.7%	IC	CU Level c	f Service	
Analysis Period (min)			15				

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Movement	EBL	EBR	NBL	NBT	SBT	SBR	
Lane Configurations				ર્સ	ţ,		
Volume (veh/h)	0	0	5	730	480	15	
Sign Control	Stop			Free	Free		
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	0	0	5	793	522	16	
Pedestrians							
Lane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)							
Median type				None	None		
Median storage veh)							
Upstream signal (ft)					66		
pX, platoon unblocked	0.89	0.89	0.89				
vC, conflicting volume	1334	530	538				
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	1315	416	425				
tC, single (s)	6.4	6.2	4.1				
tC, 2 stage (s)							
tF (s)	3.5	3.3	2.2				
p0 queue free %	100	100	99				
cM capacity (veh/h)	155	570	1015				
Direction. Lane #	NB 1	SB 1					
Volume Total	799	538					
Volume Left	5	0					
Volume Right	0	16					
cSH	1015	1700					
Volume to Capacity	0.01	0.32					
Queue Length 95th (ft)	0	0					
Control Delay (s)	0.1	0.0					
Lane LOS	A	0.0					
Approach Delay (s)	0.1	0.0					
Approach LOS		0.0					
Intersection Summary							
Average Delay			0.1				
Intersection Capacity Utiliz	zation		45.7%	IC	CU Level c	of Service	А
Analysis Period (min)			15				
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Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	f,			र्स	¥	
Volume (veh/h)	125	10	15	220	10	10
Sign Control	Free			Free	Stop	
Grade	0%			0%	0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	136	11	16	239	11	11
Pedestrians						
Lane Width (ft)						
Walking Speed (ft/s)						
Percent Blockage						
Right turn flare (veh)						
Median type	None			None		
Median storage veh)						
Upstream signal (ft)				122		
pX, platoon unblocked						
vC, conflicting volume			147		413	141
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol			147		413	141
tC, single (s)			4.1		6.4	6.2
tC, 2 stage (s)						
tF (s)			2.2		3.5	3.3
p0 queue free %			99		98	99
cM capacity (veh/h)			1435		589	907
Direction, Lane #	EB 1	WB 1	NB 1			
Volume Total	147	255	22			
Volume Left	0	16	11			
Volume Right	11	0	11			
cSH	1700	1435	714			
Volume to Capacity	0.09	0.01	0.03			
Queue Length 95th (ft)	0	1	2			
Control Delay (s)	0.0	0.6	10.2			
Lane LOS		A	В			
Approach Delay (s)	0.0	0.6	10.2			
Approach LOS			В			
Intersection Summary						
Average Delay			0.9			
Intersection Capacity Utili	zation		32.9%	IC	U Level c	of Service
Analysis Period (min)			15			
Queue Length 95th (ft) Control Delay (s) Lane LOS Approach Delay (s) Approach LOS Intersection Summary Average Delay Intersection Capacity Utili Analysis Period (min)	0 0.0 0.0 zation	1 0.6 A 0.6	2 10.2 B 10.2 B 0.9 32.9% 15	IC	CU Level c	of Service

## Queues 1: North Road & Southampton Road

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Lane Group	EBL	EBT	WBL	WBT	WBR	NBL	NBT	SBL	SBT	
Lane Configurations		4		ર્શ	1		4		\$	
Volume (vph)	20	120	160	60	70	35	215	115	205	
Lane Group Flow (vph)	0	192	0	268	85	0	543	0	351	
Turn Type	Perm		Perm		Perm	Perm		Perm		
Protected Phases		4		8			2		6	
Permitted Phases	4		8		8	2		6		
Detector Phase	4	4	8	8	8	2	2	6	6	
Switch Phase										
Minimum Initial (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	
Minimum Split (s)	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0	
Total Split (s)	30.0	30.0	30.0	30.0	30.0	35.0	35.0	35.0	35.0	
Total Split (%)	46.2%	46.2%	46.2%	46.2%	46.2%	53.8%	53.8%	53.8%	53.8%	
Yellow Time (s)	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	
All-Red Time (s)	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
Lost Time Adjust (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Total Lost Time (s)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	
Lead/Lag										
Lead-Lag Optimize?										
Recall Mode	None	None	None	None	None	Min	Min	Min	Min	
v/c Ratio		0.32		0.59	0.14		0.68		0.58	
Control Delay		11.1		18.1	4.0		13.1		13.8	
Queue Delay		0.0		0.0	0.0		0.0		0.0	
Total Delay		11.1		18.1	4.0		13.1		13.8	
Queue Length 50th (ft)		23		41	0		61		48	
Queue Length 95th (ft)		84		124	19		216		162	
Internal Link Dist (ft)		42		249			1		237	
Turn Bay Length (ft)										
Base Capacity (vph)		1243		947	1139		1349		1092	
Starvation Cap Reductn		0		0	0		0		0	
Spillback Cap Reductn		0		0	0		0		0	
Storage Cap Reductn		0		0	0		0		0	
Reduced v/c Ratio		0.15		0.28	0.07		0.40		0.32	
Intersection Summarv										
Cycle Length: 65										
Actuated Cycle Length: 41 4	4									
Natural Cycle: 45										
Control Type: Actuated-Unc	oordinated	1								
		-								

Splits and Phases: 1: North Road & Southampton Road

⊴¶ ₀2	A 04
35 s	30 s
₽	<b>∲</b> ø8
35 s	30 s

## HCM Signalized Intersection Capacity Analysis 1: North Road & Southampton Road

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			र्स	1		\$			\$	
Volume (vph)	20	120	35	160	60	70	35	215	255	115	205	20
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)		4.0			4.0	4.0		4.0			4.0	
Lane Util. Factor		1.00			1.00	1.00		1.00			1.00	
Frt		0.97			1.00	0.85		0.93			0.99	
Flt Protected		0.99			0.96	1.00		1.00			0.98	
Satd. Flow (prot)		1803			1763	1553		1730			1817	
Flt Permitted		0.95			0.72	1.00		0.96			0.74	
Satd. Flow (perm)		1722			1320	1553		1667			1370	
Peak-hour factor, PHF	0.91	0.91	0.91	0.82	0.82	0.82	0.93	0.93	0.93	0.97	0.97	0.97
Adj. Flow (vph)	22	132	38	195	73	85	38	231	274	119	211	21
RTOR Reduction (vph)	0	15	0	0	0	55	0	59	0	0	4	0
Lane Group Flow (vph)	0	177	0	0	268	30	0	484	0	0	347	0
Heavy Vehicles (%)	2%	2%	2%	4%	4%	4%	2%	2%	2%	2%	2%	2%
Turn Type	Perm			Perm		Perm	Perm			Perm		
Protected Phases		4			8			2			6	
Permitted Phases	4			8		8	2			6		
Actuated Green, G (s)		14.3			14.3	14.3		18.3			18.3	
Effective Green, g (s)		14.3			14.3	14.3		18.3			18.3	
Actuated g/C Ratio		0.35			0.35	0.35		0.45			0.45	
Clearance Time (s)		4.0			4.0	4.0		4.0			4.0	
Vehicle Extension (s)		3.0			3.0	3.0		3.0			3.0	
Lane Grp Cap (vph)		607			465	547		751			618	
v/s Ratio Prot												
v/s Ratio Perm		0.10			c0.20	0.02		c0.29			0.25	
v/c Ratio		0.29			0.58	0.05		0.64			0.56	
Uniform Delay, d1		9.5			10.7	8.7		8.6			8.2	
Progression Factor		1.00			1.00	1.00		1.00			1.00	
Incremental Delay, d2		0.3			1.7	0.0		1.9			1.2	
Delay (s)		9.8			12.4	8.7		10.5			9.4	
Level of Service		А			В	А		В			А	
Approach Delay (s)		9.8			11.5			10.5			9.4	
Approach LOS		А			В			В			А	
Intersection Summary												
HCM Average Control Delay			10.4	Н	CM Level	l of Servic	е		В			
HCM Volume to Capacity ratio			0.61									
Actuated Cycle Length (s)			40.6	S	um of los	t time (s)			8.0			
Intersection Capacity Utilization	า		82.1%	IC	CU Level of	of Service			Е			
Analysis Period (min)			15									

c Critical Lane Group

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Movement	EBL	EBR	NBL	NBT	SBT	SBR	
Lane Configurations	Y			र्स	et.		
Volume (veh/h)	20	30	25	495	380	5	
Sign Control	Stop			Free	Free		
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	22	33	27	538	413	5	
Pedestrians							
Lane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)							
Median type				None	None		
Median storage veh)							
Upstream signal (ft)					258		
pX, platoon unblocked							
vC, conflicting volume	1008	416	418				
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	1008	416	418				
tC, single (s)	6.4	6.2	4.1				
tC, 2 stage (s)							
tF (s)	3.5	3.3	2.2				
p0 queue free %	92	95	98				
cM capacity (veh/h)	260	637	1141				
Direction, Lane #	EB 1	NB 1	SB 1				
Volume Total	54	565	418				
Volume Left	22	27	0				
Volume Right	33	0	5				
cSH	403	1141	1700				
Volume to Capacity	0.13	0.02	0.25				
Queue Length 95th (ft)	12	2	0				
Control Delay (s)	15.3	0.7	0.0				
Lane LOS	С	А					
Approach Delay (s)	15.3	0.7	0.0				
Approach LOS	С						
Intersection Summary							
Average Delav			1.2				
Intersection Capacity Utilizat	ion		56.4%	IC	CU Level c	of Service	
Analysis Period (min)			15				

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Movement	EBL	EBR	NBL	NBT	SBT	SBR	
Lane Configurations				र्स	eî.		
Volume (veh/h)	0	0	10	505	385	15	
Sign Control	Stop			Free	Free		
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	0	0	11	549	418	16	
Pedestrians							
Lane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)							
Median type				None	None		
Median storage veh)							
Upstream signal (ft)					66		
pX, platoon unblocked	0.93	0.93	0.93				
vC, conflicting volume	997	427	435				
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	960	347	356				
tC, single (s)	6.4	6.2	4.1				
tC, 2 stage (s)							
tF (s)	3.5	3.3	2.2				
p0 queue free %	100	100	99				
cM capacity (veh/h)	262	648	1120				
Direction, Lane #	NB 1	SB 1					
Volume Total	560	435					
Volume Left	11	0					
Volume Right	0	16					
cSH	1120	1700					
Volume to Capacity	0.01	0.26					
Queue Length 95th (ft)	1	0					
Control Delay (s)	0.3	0.0					
Lane LOS	А						
Approach Delay (s)	0.3	0.0					
Approach LOS							
Intersection Summary							
Average Delay			0.2				
Intersection Capacity Utilizat	ion		37.9%	IC	CU Level c	of Service	
Analysis Period (min)			15				

	-	$\mathbf{\hat{z}}$	4	+	1	1	
Movement	EBT	EBR	WBL	WBT	NBL	NBR	
Lane Configurations	4Î			र्स	¥		
Volume (veh/h)	155	15	20	95	15	20	
Sign Control	Free			Free	Stop		
Grade	0%			0%	0%		
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	
Hourly flow rate (vph)	168	16	22	103	16	22	
Pedestrians							
Lane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)							
Median type	None			None			
Median storage veh)							
Upstream signal (ft)				122			
pX, platoon unblocked							
vC, conflicting volume			185		323	177	
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol			185		323	177	
tC, single (s)			4.1		6.4	6.2	
tC, 2 stage (s)							
tF (s)			2.2		3.5	3.3	
p0 queue free %			98		98	97	
cM capacity (veh/h)			1390		660	866	
Direction, Lane #	EB 1	WB 1	NB 1				
Volume Total	185	125	38				
Volume Left	0	22	16				
Volume Right	16	0	22				
cSH	1700	1390	764				
Volume to Capacity	0.11	0.02	0.05				
Queue Length 95th (ft)	0	1	4				
Control Delay (s)	0.0	1.4	10.0				
Lane LOS		А	А				
Approach Delay (s)	0.0	1.4	10.0				
Approach LOS			A				
Intersection Summary							
Average Delay			1.6				
Intersection Capacity Utilization	n		28.5%	IC	U Level o	f Service	
Analysis Period (min)			15				

Cumberland Farms Concept Plan

Parking Summary Chart									
	Si	ces							
Description	Required	Provided	Required	Provided					
STANDARD SPACES	9 x 19	9 x 19	15	24					
STANDARD ACCESSIBLE SPACES *	15 x 19	15 x 19	1	1					
VAN ACCESSIBLE SPACES	16 x 19	16 x 19	1	1					
TOTAL SPACES			16	26					
LOADING BAYS**			_	_					

RETAIL\*

\* ADA/STATE/LOCAL REQUIREMENTS: 1 VAN SPACE AND 1 STANDARD SPACE REQUIRED FOR 26 TO 50 PARKING SPACES PROVIDED.

\*\* LOADING BAYS: FOR ONE LOADING BAY MIN. BUILDING AREA OF 25,000 SF IS REQUIRED. NO LOADING BAY IS REQUIRED.

Parking Requirements:

4,513 SF x 1 SPACES / 300 SF GFA = 15.04 SPACES TOTAL PARKING REQUIRED = 16 SPACES

Zoning Summary Chart							
Zoning District(S):	BUSINESS – B						
Overlay District(S):	NONE						
Zoning Regulation Requirements	Required	Provided					
MINIMUM LOT SIZE	12,000 SF	50,944 SF (1.17 AC)					
MINIMUM LOT FRONTAGE (NORTH ROAD)	100 FT	177 FT					
MAXIMUM BUILDING COVERAGE	80%	8.9% (EXCLUDES GAS CANOPY)					
FRONT YARD SETBACK: SOUTHAMPTON ROAD	30 Feet	31.0 Feet (CANOPY)					
FRONT YARD SETBACK: NORTH BLVD	30 Feet	72.4 Feet (CANOPY)					
SIDE YARD SETBACK	20 Feet	67 Feet (CANOPY)					
REAR YARD SETBACK	20 Feet	20.5 Feet (BUILDING O⊢					
MAXIMUM BUILDING HEIGHT	2.5 STORIES/ 35FT	30.83 Feet					

Signage Summary Chart								
Zoning Regulation Requirements	Allowed	Provided						
FREE-STANDING (PYLON) SIGN - AREA	40 SF PER SIDE	40 SF PER SIDE						
FREE-STANDING SIGN (PYLON) - HEIGHT	22FT	22FT						
CANOPY SIGN – AREA	TBD **	11 SF (x2)						
BUILDING SIGN – AREA	279.19 SF/ 177 SF *	37.6 SF/ 27.8 SF						

\* ACCESSORY SIGN: PER SEC. 8-10.2: MAX OVERALL SIZE OF PERMITTED ACCESSORY WALL SIGNS MAY NOT EXCEED 1 SF PER 1 LF OF FRONTAGE ON A STREET OR PUBLIC PEDESTRIAN WAY: SOUTHAMPTON ROAD: 279.19 FT = 279.19 SF SIGN NORTH ROAD: 177 LF = 177 SF SIGN

\*\* FURTHER INVESTIGATION REQUIRED WITH MUNICIPALITY

<b>On-Site Traffic Signage Chart</b>								
MUTCD	Specif	ication	D					
Number	Width	Height	Desc.					
R1-1	30"	30"	STOP					
R7-8	12"	18"	HANDICAPPED PARKING PROCEMENT OF ALE MATTOCARD OF ALE MATTOCARD OF ALE MATTOCARD OF ALE MATTOCARD OF ALE MATTOCARD OF ALE					
R7-8a	12"	6"	VAN					



No.	Revision		Date	Appvd.
Designed by Drawn by			Checked by	
CAD checked by		Approved by		
Scale 1"=20'		Date January 31, 2013		

## Proposed Cumberland Farms Convenience Store with Gas

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